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Thereof ...

MAIL STOP

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VERIFICATION OF TRANSLATION

I, Yukiko Uetake, hereby declare that:

My name and residence address are as stated below.

I am proficient in both the Japanese and English languages, and have translated Japanese Application 2003-280373, which is in the Japanese language, into English. A copy of the English translation is submitted herewith. I verify that this English translation is both true and complete.

All statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Date: March 23, 2009

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JAPAN PATENT OFFICE

This is to certify that the annexed is a true copy of
the following application as filed with this office.

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Application Number: 2003-280373

Applicant(s): Nippon Shokubai Co., Ltd.

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Hiroshi OGAWA

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【Name of thing】	Claim	1
【Name of thing】	Specification	1
【Name of thing】	Abstract	1

[Name of Document] Specification

[Scope of Claim for a Patent]

[Claim 1] A water-absorbent resin composition,
comprising:

5 (A) cross-linked absorbent resin obtainable by polymerizing
an unsaturated monomer having an acid group and/or a salt thereof
as main component; and

(B) complex oxide hydrate containing (b1) zinc and silicon,
or (b2) zinc and aluminum,

10 wherein the complex oxide hydrate contains zinc as main
metal component,

the mass ratio of the content of zinc and the content of
silicon or aluminum is in the range of 50/50 - 99/1, and

the absorption capacity at 60 minutes toward 0.90 mass%
15 sodium chloride aqueous solution under the pressure of 1.9 kPa
is not less than 20 g/g.

[Claim 2] A water-absorbent resin composition
according to claim 1, wherein (B) the complex oxide hydrate is
obtained by co-precipitation method in a solution containing
20 a water-soluble zinc compound and a water-soluble silicon
compound or in a solution containing a water-soluble zinc
compound and a water-soluble aluminum compound.

[Claim 3] A water-absorbent resin composition
according to claim 1 or claim 2, wherein the separation ratio
25 of the complex oxide hydrate from the water-absorbent resin in
a swollen state is not more than 20%.

[Claim 4] A water-absorbent resin composition
according to any one of claim 1 - 3, wherein the water-absorbent
resin composition is in a granular state and contains particles
30 exceeding 150 μm and not exceeding 850 μm in diameter in a
proportion of not less than 90 mass% of all the particles and
particles exceeding 300 μm in diameter in a proportion of not

less than 60 mass% of all the particles.

[Claim 5] A water-absorbent resin composition according to any one of claim 1 - 4, further comprising a plant component.

5 [Claim 6] An absorbent material for sanitary product comprising:

the water-absorbent resin composition of any one of claim 1 - 5; and
hydrophilic fibers.

10 [Claim 7] An absorbent material for sanitary product comprising (A) water-absorbent resin including (A) cross-linked water-absorbent resin obtainable by polymerizing an unsaturated monomer containing an acid group and/or a salt thereof as main component, and hydrophilic fiber, wherein

15 the absorbent material includes (B) complex oxide hydrate containing (b1) zinc and silicon, or (b2) zinc and aluminum, wherein (B) the complex oxide hydrate contains zinc as main metal component,

the mass ratio of the content of zinc and the content of
20 silicon or aluminum is in the range of 50/50 - 99/1, and

the absorption capacity at 60 minutes toward 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa is not less than 20 g/g,

[Claim 8] An absorbent product comprising:

25 the absorbent material of claim 6 or 7,
topsheet possessing permeability to liquid; and
backsheet possessing impermeability to liquid.

[Claim 9] A method for producing water-absorbent resin composition including (A) cross-linking absorbent resin
30 obtainable by polymerizing an unsaturated monomer having an acid group and/or a salt thereof as main component; and (B) complex oxide hydrate containing (b1) zinc and silicon, or (b2) zinc

and aluminum, comprising the steps of:

obtaining a water-absorbent resin by polymerizing an unsaturated monomer containing an acid group as main component;

5 mixing the water-absorbent resin and (B) complex oxide hydrate; and

the absorbent resin obtained through the polymerization step has not less than 20 g/g of absorption capacity at 60 minutes toward 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9kPa.

[Name of Document] Specification

[Title of the Invention] WATER-ABSORBENT RESIN COMPOSITION AND
METHOD FOR PRODUCING THEREOF, AND ABSORBENT MATERIAL AND
ABSORBENT PRODUCT USING THEREOF

5 [Detailed Description of the Invention]

[0001]

[Technical Field to which the invention pertains]

This invention relates to a water-absorbent resin
composition, an absorbent material, and an absorbent product,
10 and a method for the production of the water-absorbent resin
composition. More particularly, this invention relates to a
water-absorbent resin composition, an absorbent material, and
an absorbent product which exhibit excellent hygroscopic and
fluid property, separation-resistant property, deodorizing
15 property, gel strength and absorbent property, when used as
sanitary materials such as disposable diapers, sanitary napkins,
and incontinence pads. This invention further relates to a
method for the production of a water-absorbent resin composition
possessing such characteristics.

20 [Prior Art]

[0002]

The water-absorbent resin is extensively used in such
sanitary materials as disposable diapers, sanitary napkins, and
incontinence pads with the object of absorbing such humors as
25 urine and blood and form main components of such sanitary
materials as these.

[0003]

In recent years, in consequence of growth in the demand
for adult disposable diapers owing particularly to the aging
30 of the society, the desirability of imparting a deodorizing
property, particularly a deodorizing property capable of
eliminating offensive odors originating in such sulfur type

compounds as hydrogen sulfide and mercaptans, to the water-absorbent resin has been finding growing recognition.

[0004]

As a means to impart the deodorizing property to the
5 water-absorbent resin, the combinations of the water-absorbent resin with various kinds of deodorants and antibacterial agents have been proposed. For example, a water-absorbent resin composition comprising a water-absorbent resin and the extract of leaves of the trees of theaceous plant (refer to patent
10 reference 1, for example), an adsorbent resin composition containing the extract of coniferous trees and a water-absorbent resin possessing a specific performance (refer to patent reference 2, for example), a deodorizing resin composition having zeolite particles dispersed in a water-absorbent resin (refer
15 to patent reference 3, for example), a water-absorbent resin composition formed of a water-absorbent resin and a metal-containing hydroxide comprising one element selected among titanium and zirconium and at least one element selected among zinc, aluminum, calcium, magnesium, and silicon (refer to patent
20 reference 4, for example), a water-absorbent resin composition formed of a water-absorbent resin, an oxalate compound, and a complex silicate compound (refer to patent reference 5), a water-absorbent resin composition formed of a water-absorbent resin, a tannate, and a complex silicate compound (refer to patent
25 reference 6, for example), a water-absorbent resin composition formed of a water-absorbent resin, a glycine type amphoteric surfactant, and a complex silicate compound (refer to patent reference 7, for example), and a water-absorbent resin composition formed of a water-absorbent resin, a
30 sulfur-containing reducing agent, and a complex silicate compound (refer to patent reference 8, for example) have been known.

[0005]

Methods for imparting a deodorizing property to absorbent products using a water-absorbent resin also have been being studied. For example, an absorbent product formed of refined
5 tea and a water-absorbent resin (refer to patent reference 9, for example), a disposable diaper containing a water-absorbent resin and a resin formed of benzalkonium chloride and/or chlorohexidine gluconate (refer to patent reference 10, for example), and a sanitary store combining a water-absorbent resin
10 and zinc aluminosilicate (refer to patent reference 11, for example) have been known.

[0006]

The feasibility of imparting a deodorizing property and a powder handling property both to a water-absorbent resin also
15 has been being studied. For example, an absorbent agent formed of a water-absorbent resin, a compound possessing an antibacterial function against an ammonia-producing microbe, and a pharmaceutical preparation manifesting a neutralizing ability or a neutralizing ability and an adsorbing ability to
20 ammonia (refer to patent reference 12, for example) has been known. As concerns the water-absorbent resin, the improvement in the hygroscopic and fluid property (the improvement in the anti-caking property) forms an important task besides the impartation of a deodorizing property and an anti-bacterial
25 property to the water-absorbent resin. To be specific, the water-absorbent resin has the problem of losing fluidity as powder and entailing the phenomenon of blocking during the course of absorbing humidity. The patent reference 12 also discloses a technique of using various additives for the purpose of solving
30 this problem.

When the water-absorbent resin incorporates additives therein for the purpose of enhancing the deodorant property and the

hygroscopic and fluid property, it possibly entails such adverse phenomena as separation and exfoliation where the additives are in the form of powder. When the separation or exfoliation of such additives occurs, the additives entail formation of dust and fail to manifest the function thereof fully satisfactorily.

[0007]

The deodorizing property produced by any of the aforementioned hitherto reported methods is not so great as to reach the level of manifesting a fully satisfactory deodorization in actual use.

[0008]

When the water-absorbent resin sacrifices the absorbent property thereof for the sake of enabling the deodorizing property thereof to be manifested to a high degree, it does not achieve the inherent object of absorbing such humors as urine and blood. It is, therefore, an important rule to have the absorbent property exalted to a fully satisfactory level while having the deodorizing property manifested to a high degree as well.

[0009]

[Patent Reference 1]
JP-A-S60-158861

[0010]

[Patent Reference 2]
JP-A-H11-241030

[Patent Reference 3]
JP-A-H08-176338

[Patent Reference 4]
JP-A-H10-147724

[Patent Reference 5]
JP-A-H10-298442

[Patent Reference 6]
JP-A-H11-116829

[Patent Reference 7]

JP-A-H11-49971

[Patent Reference 8]

JP-A-H11-148023

5 [Patent Reference 9]

JP-A-H2-41155

[Patent Reference 10]

JP-A-S63-135501

[Patent Reference 11]

10 JP-A-S64-5546

[Patent Reference 12]

International Publication WO00/01479

[Problem to be solved by the Invention]

[0011]

15 An object of this invention is to provide a water-absorbent resin composition, an absorbent material, and an absorbent product, and a method for production of a water-absorbent resin composition, which relate to a water-absorbent resin composition including a water-absorbent resin and an additive, which have
20 a low ratio of separation of additives (low separation ratio), excel in the hygroscopic and fluid property (fluid property of a powder after water-absorbent resin or water-absorbent resin absorbed water) and in the deodorizing property (especially, odor originating in sulfur compounds such as hydroge disulfide
25 or mercaptan), and also excel in the absorbent property.

[Means for Solving Problem]

[0012]

The present inventor has pursued a diligent study with a view to solving the task mentioned above. He has consequently
30 taken notice of the fact that the combination of a water-absorbent resin and zinc is effective in manifesting a deodorizing property. He has made a diligent study in search of conditions for enhancing

the deodorizing property and enabling the excellent absorbent property and the excellent hygroscopic and fluid property to be manifested fully. He has finally found that the task can be solved by combining a water-absorbent resin possessing a prescribed absorbent property and (B) a complex oxide hydrate containing zinc and silicon or zinc and aluminum at a prescribed ratio and using a water-absorbent resin with a cross-linked structure which has a prescribed absorbent property as the water-absorbent resin.

10 [0013]

Specifically, this invention concerns a water-absorbent resin composition having the absorption capacity (60 minutes) toward 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa not less than 20 g/g, comprising: (A) absorbent resin obtainable by polymerizing an unsaturated monomer having an acid group and/or a salt thereof; and (B) complex oxide hydrate containing (b1) zinc and silicon, or (b2) zinc and aluminum, wherein (B) the complex oxide hydrate contains zinc as main metal component, and the mass ratio of the content of zinc and the content of silicon or aluminum is in the range of 50/50 - 99/1.

[0014]

Further, this invention concerns an absorbent material comprising the water-absorbent resin composition mentioned above, and hydrophilic fibers.

25 [0015]

This invention further concerns an absorbent material comprising: (A) water-absorbent resin obtainable by polymerizing an unsaturated monomer containing an acid group and/or a salt thereof as main component; and (B) complex oxide hydrate containing (b1) zinc and silicon, or (b2) zinc and aluminum, wherein (B) the complex oxide hydrate contains zinc as main metal component, the mass ratio of the content of zinc and the content

of silicon or aluminum is in the range of 50/50 - 99/1, and the water-absorbent resin has the absorption capacity at 60 minutes toward 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa not less than 20 g/g,

5 [0016]

This invention concerns an absorbent product comprising the absorbent material mentioned above, topsheet possessing permeability to liquid; and backsheet possessing impermeability to liquid.

10 This invention also concerns a method for producing water-absorbent resin composition which includes (A) water-absorbent resin obtainable by polymerizing an unsaturated monomer containing an acid group and/or a salt thereof as a main component; and (B) complex oxide hydrate containing (b1) zinc
15 and silicon, or (b2) zinc and aluminum, which comprises the steps of: polymerizing an unsaturated monomer containing an acid group thereby obtaining a water-absorbent resin having not less than 20 g/g of absorption capacity at 60 minutes toward 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa;
20 and mixing the water-absorbent resin and (B) complex oxide hydrate containing zinc and silicon, or zinc and aluminum.

[0017]

The water-absorbent resin composition, the absorbent material, and the absorbent product, and a method for production
25 water-absorbent resin composition provided by the present invention can show excellent deodorant property with regard to hydrogen disulfide, ammonia, deodorant test, separation ratio, and blocking ratio, and can suffer only a low ratio of separation of additives from water-absorbent resin, excel in hygroscopic
30 and fluid property and deodorizing property.

[Detailed Description of the Invention]

[0018]

(1) Water-absorbent resin (A)

The term "absorbent resin" (A) as used in this invention refers to a cross-linked polymer which is capable of forming a hydrogel and manifesting water-swelling property and water insolubility. The term "water-swelling property" refers to the ability of the water-absorbent resin in deionized water to absorb the water in a large amount of not less than 5 times, preferably 50 times to 1000 times, its own weight. The term "water insolubility" refers to the fact that the content of the uncross-linked water-soluble component (water-soluble polymer) in the water-absorbent resin (A) is preferably not more than 50 mass% (lower limit: 0 mass%), more preferably not more than 25 mass%, still more preferably not more than 20 mass%, and particularly preferably not more than 15 mass%, and most preferably not more than 10 mass%. Incidentally, the method for determining this water-soluble component is described in Edana Recommended Test Methods 470, 1 - 99 Extractables of European Disposables and Nonwovens Association.

[0019]

When the content ratio based on the water-absorbent resin in is mentioned in the description of the invention, it is based on the solids content of the water-absorbent resin (it is calculated as the content ratio which is obtained, for example, by drying 1 g of water-absorbent resin for three hours so as to lower the water content thereof to not more than 10 mass%).

[0020]

As the water-absorbent resin (A) in this invention, the water-absorbent resin which results from polymerizing an unsaturated monomer containing an acid group and/or a salt thereof and possesses a cross-linked structure is used from the viewpoint of deodorizing property and absorbent property.

[0021]

As the water-absorbent resin (A), one or more compounds selected from the group consisting of partially neutralized polymer of polyacrylic acid; hydrolyzate of starch-acrylonitrile graft polymer; starch-acrylic acid graft polymer; saponified vinyl acetate-acrylic ester copolymer; hydrolyzate of acrylonitrile copolymer or acrylamide copolymer or cross-linked product thereof; modified carboxyl group-containing cross-linked polyvinyl alcohol; and cross-linked isobutylene-maleic anhydride copolymer may be used. Preferably, as the water-absorbent resin (A), the partially neutralized polymer of polyacrylic acid which is obtained by polymerizing and cross-linking a monomer component having acrylic acid and/or a salt (product of neutralization) thereof as a main component is used.

[0022]

The water-absorbent resin (A) possesses an acid group and/or a salt thereof. Preferably, the water-absorbent resin (A) is obtained by polymerizing a monomer component having an acid group-containing unsaturated monomer as a main component. The acid group-containing unsaturated monomer includes a monomer (for example, acrylonitrile) which is transformed into an acid group by undergoing hydrolysis subsequent to polymerization. Preferably, the acid group-containing unsaturated monomer which contains the acid group during the course of polymerization is used.

[0023]

In this invention, the monomer component is preferred to have acrylic acid and/or a salt thereof as a main component.

[0024]

When the monomer component has acrylic acid and/or a salt thereof as a main component, it may use other monomer in combination therewith. The monomer to be used in this

combination does not need to be particularly restricted but is only required to ensure manifestation of the effect of this invention. As concrete examples of the monomer useful for this purpose, such water-soluble or hydrophobic unsaturated monomers
5 as methacrylic acid, maleic acid, maleic anhydride, fumaric acid, crotonic acid, itaconic acid, vinyl sulfonic acid, 2-(meth)acrylamide-2-methylpropane sulfonic acid, (meth)acryloxyalkane sulfonic acid, and alkali metal salts thereof, and ammonium salts, N-vinyl-2-pyrrolidone, N-vinyl
10 acetamide, (meth)acrylamide, N-isopropyl (meth)acrylamide, N,N-dimethyl (meth)acrylamide, 2-hydroxyethyl (meth)acrylate, methoxypolyethylene glycol (meth)acrylate, polyethylene glycol (meth)acrylate, isobutylene, and lauryl (meth)acrylate may be cited.

15 [0025]

When a monomer other than acrylic acid and/or a salt thereof is used, the ratio of the monomer other than acrylic acid and/or the salt thereof is preferably 0 - 30 mol% and more preferably not more than 10 mol% based on the total amount of the acrylic
20 acid and/or the salt thereof. By using the monomer in this ratio, the performance of absorption of the produced water-absorbent resin is further enhanced. The use of this monomer allows the water-absorbent resin to be obtained more inexpensively. Further, the effect of this invention can be manifested
25 satisfactorily.

[0026]

The water-absorbent resin (A) possesses a cross-linked structure. The cross-linked structure may be a self-cross-linked type using no cross-linking agent.
30 Preferably, a cross-linked structure which is formed by the copolymerization or reaction using a cross-linking agent possessing two or more polymerizing unsaturated groups or two

or more reactive groups within the molecular unit is used.

[0027]

As concrete examples of the inner cross-linking agent, N,N'-methylenebis(meth)acrylamide, (poly)ethylene glycol di(meth)acrylate, (poly)propylene glycol di(meth)acrylate, trimethylol propane tri(meth)acrylate, glycerin tri(meth)acrylate, glycerin acrylate methacrylate, ethylene oxide-modified trimethylol propane tri(meth)acrylate, pentaerythritol hexa(meth)acrylate, triallyl cyanurate, triallyl isocyanurate, triallyl phosphate, triallyl amine, poly(meth)allyloxy alkane, (poly)ethylene glycol diglycidyl ether, glycerol diglycidyl ether, ethylene glycol, polyethylene glycol, propylene glycol, glycerin, pentaerythritol, ethylene diamine, ethylene carbonate, propylene carbonate, polyethylene imine, and glycidyl (meth)acrylate may be cited.

[0028]

The inner cross-linking agents may be used either singly or in the form of a proper mixture of two or more members. The inner cross-linking agents may be added collectively at once or piecemeal to the reaction system. When the inner cross-linking agent is used, it is favorable to use a compound possessing two or more polymerizing unsaturated group during polymerization for the purpose of enabling the effect of this invention to be fully manifested.

[0029]

The amount of the inner cross-linking agent to be used is preferably in the range of 0.001 - 2 mol%, more preferably 0.005 - 0.5 mol%, still more preferably 0.01 - 0.2 mol%, and particularly preferably 0.03 - 0.15 mol% based on the amount of the monomer component (excluding the cross-linking agent). If the amount of the inner cross-linking agent to be used falls short of 0.001 mol% or exceeds 2 mol%, the deviation from the limits may possibly

prevent the produced water-absorbent resin from manifesting the absorbent property fully satisfactorily. It may also possibly prevent the effect of this invention from being fully manifested.

[0030]

5 The introduction of the cross-linked structure into the polymer by the use of the inner cross-linking agent may be accomplished by adding the inner cross-linking agent to the reaction system before, during, or after the polymerization of the monomer component or after the neutralization thereof.

10 [0031]

As means to polymerize the monomer component for the purpose of obtaining the water-absorbent resin (A), aqueous solution polymerization, reversed-phase suspended polymerization, bulk polymerization, and precipitation polymerization, for example,
15 are available. From the viewpoint of such factors as the performance, the ease of control of the polymerization, and the absorbent property of the swelled gel, the aqueous solution polymerization or the reversed-phase suspended polymerization performed in an aqueous solution containing the monomer component
20 proves advantageous.

[0032]

The concentration of the monomer component in the aqueous solution containing the monomer component (hereinafter occasionally referred to as "aqueous monomer solution") is not
25 particularly restricted but may be decided by the temperature of the aqueous solution and the kind of the monomer component. The concentration of the monomer component is preferably in the range of 10 - 70 mass% and more preferably 20 - 60 mass%. When the aqueous solution polymerization is performed, a solvent other
30 than water may be additionally used as occasion demands. The kind of solvent which is so used additionally is not particularly restricted.

[0033]

The reversed-phase suspension polymerization is a method of polymerization which requires the aqueous monomer solution to be suspended in a hydrophobic organic solvent. The reversed-phase suspended polymerization is disclosed, for example, in U.S. Patent No. 4093776, U.S. Patent No. 4367323, U.S. Patent No. 4446261, U.S. Patent No. 4683274, and U.S. Patent No. 5244735. The aqueous solution polymerization is a method of polymerizing the aqueous monomer solution without using a dispersing solvent. The aqueous solution polymerization is disclosed, for example, in such U.S. patents as U.S. Patent 4625001, U.S. Patent No. 4873299, U.S. Patent No. 4286082, U.S. Patent No. 4973632, U.S. Patent No. 4985518, U.S. Patent No. 5124416, U.S. Patent No. 5250640, U.S. Patent No. 5264495, U.S. Patent No. 5145906, and U.S. Patent No. 5380808 and such European patents as European Patent No. 0811636, European Patent No. 0955086, and European Patent No. 0922717. The monomer components and the initiating agents which are cited in these methods of polymerization may be adopted for the present invention.

[0034]

In initiating the polymerization, such radical polymerization initiators as potassium persulfate, ammonium persulfate, sodium persulfate, t-butyl hydroperoxide, hydrogen peroxide, and 2,2'-azobis(2-amidinopropane) dihydrochloride; and such photopolymerization initiators as 2-hydroxy-2-methyl-1-phenyl-propan-1-one may be used. The amount of the polymerization initiator to be used is preferably in the range of 0.001 - 2 mol%, and more preferably 0.01 - 0.1 mol% (based on the total monomer component) in consideration of physical properties of the produced water-absorbent resin.

[0035]

By performing the polymerization, generally a hydrogel type

cross-linked polymer is obtained. This hydrogel type cross-linked polymer is optionally divided finely, and dried, then preferably pulverized before and/or after the drying to obtain the water-absorbent resin.

5 [0036]

The drying is effected at a temperature preferably in the range of 60°C - 250°C, more preferably 100°C - 220°C, and still more preferably 120°C - 200°C. The drying time is selected, depending on the surface area and the water content of the polymer
10 and the kind of the drying device, so as to control a target water content of the water-absorbent resin.

[0037]

The water content of the water-absorbent resin (A) is not particularly restricted (the water content of the
15 water-absorbent resin is determined as the amount of water contained in the water-absorbent resin. It is determined, for example, as the amount of loss to be found by drying 1 g of a given water-absorbent resin at 180°C for three hours.). For the purpose of ensuring the effect of this invention to be manifested
20 satisfactorily, the water-absorbent resin (A) is preferred to be in the form of a powder capable of manifesting fluidity even at room temperature. The water content of the water-absorbent resin (A) is preferably 0.2 - 30 mass%, more preferably 0.3 - 15 mass%, and still more preferably 0.5 - 10 mass%. The
25 water-absorbent resin (A) is preferably in the form of powder.

[0038]

Since it is difficult to decrease to zero the water content of the water-absorbent resin, it is permissible to use the water-absorbent resin in the form of powder which contains a
30 small amount of water (for example, 0.5 - 10 mass%), and such a water-absorbent resin is also called "water-absorbent resin (A)" herein. When the properties specified in the present

specification are determined with respect to the water-absorbent resin (the water-absorbent resin composition) which are commercially available or the water-absorbent resin (the water-absorbent resin composition) which are actually used in disposable diapers, they are determined after a given sample has been dried till the water content decreases to not more than 10 mass% or it is preferably adjusted to 5 ± 2 mass%. The drying conditions for the sake of adjusting the water content do not need to be particularly restricted but are only required to avoid inducing the water-absorbent resin or the water-absorbent resin composition to sustain any decomposition or denaturation. Preferably, the drying may be performed under reduced pressure.

[0039]

The particulate shape of the water-absorbent resin (A) is not particularly restricted. The particulates of the water-absorbent resin (A) may assume the shape of spheres, crushed fragments, or amorphous grains, for example. The water-absorbent resin is preferred to be in the shape of amorphously crushed grains which are obtained through the pulverizing step. The bulk density of the water-absorbent resin (A) specified in JIS (Japanese Industrial Standard) K-3362, for the sake of enabling the effect of this invention to be satisfactorily manifested, is preferably in the range of 0.40 - 0.80 g/ml, more preferably in the range of 0.50 - 0.75 g/ml, and still more preferably 0.60 - 0.73 g/ml.

[0040]

The water-absorbent resin (A) which can be used in this invention is preferred to have further undergone a surface cross-linking (secondary cross-linking) treatment.

[0041]

Various cross-linking (surface cross-linking) agents are available for the purpose of performing the surface cross-linking

treatment and do not need to be particularly restricted. From the viewpoint of enhancing the properties of the produced water-absorbent resin, polyhydric alcohol compounds; epoxy compounds; polyamine compounds; and condensates thereof with
5 haloepoxy compounds; oxazoline compounds; mono-, di-, and poly-oxazolidinone compounds; polyvalent metal salts; and alkylene carbonate compounds are advantageously used.

[0042]

Though the surface cross-linking agent to be used does not
10 need to be particularly restricted, such surface cross-linking agents as cited in U.S. Patent No. 6228930, U.S. Patent No. 6071976, and U.S. Patent No. 6254990 are available. As concrete examples of the surface cross-linking agent, polyhydric alcohol compounds such as mono-, di-, tri-, tetra- or polyethylene glycol,
15 monopropylene glycol, 1,3-propane diol, dipropylene glycol, 2,3,4-trimethyl-1,3-pentane diol, polypropylene glycol, glycerin, polyglycerin, 2-butene-1,4-diol, 1,4-butane diol, 1,3-butane diol, 1,5-pentane diol, 1,6-hexane diol, and 1,2-cyclohexane dimethanol; epoxy compounds such as ethylene
20 glycol diglycidyl ether and glycidol; polyamine compounds such as ethylenediamine, diethylenetriamine, triethylenetetramine, tetraethylene pentamine, pentaethylene hexamine, polyethylene imine, and polyamide polyamine; haloepoxy compounds such as epichlorohydrin, epibromohydrin, and α -methylepichlorohydrin;
25 condensates of the polyamine compounds mentioned above and the haloepoxy compounds mentioned above; oxazolidinone compounds such as 2-oxazolidinone; and alkylene carbonate compounds such as ethylene carbonate may be cited. These surface cross-linking agents may be used either singly or in the form of a mixture
30 of two or more members. For the purpose of ensuring the effect of this invention to be satisfactorily manifested, it is advantageous to use a polyhydric alcohol as the surface

cross-linking agent. The polyhydric alcohol is preferred to be on the level of having 2 - 10 carbon atoms, preferably 3 - 8 carbon atoms.

[0043]

5 The amount of the surface cross-linking agent to be used is preferably in the range of 0.001 - 10 mass%, and more preferably 0.01 - 5 mass%, based on the amount of the water-absorbent resin (A), though it is variable with the kinds of compound to be used and the combination thereof.

10 [0044]

When the surface cross-linking is performed, it is preferable to use water. The amount of water to be used is preferably in the range of 0.5 - 20 mass%, and more preferably 0.5 - 10 mass%, based on the amount of the water-absorbent resin (A), though it depends on the water content of the water-absorbent resin (A) to be used. It is permissible to use a hydrophilic organic solvent besides water. When a hydrophilic organic solvent is used, the amount thereof is preferably in the range of 0 - 10 mass%, more preferably 0 - 5 mass%, and still more preferably 0 - 3 mass%, based on the amount of the water-absorbent resin (A).

[0045]

The surface cross-linking is preferably effected by a method which comprises premixing water and/or a hydrophilic organic solvent and a surface cross-linking agent and subsequently causing the resultant aqueous solution to be mixed with the water-absorbent resin by spraying or dropwise addition. A method which resorts to spraying is adopted more preferably. The drops used for the spraying preferably have an average particle diameter in the range of 0.1 - 300 μm and more preferably 0.1 - 200 μm . When water and/or a hydrophilic organic solvent is mixed with the surface cross-linking agent, the mixture may be carried out

in the presence of a water-insoluble fine powder or a surfactant on the condition that their existence does not obstruct the effect of this invention.

[0046]

5 The water-absorbent resin which has been mixed with the surface cross-linking agent is preferably subjected to a heating treatment. The heating temperature (the thermal medium temperature or the material temperature) is preferably in the range of 100 - 250°C and more preferably 150 - 250°C. The heating
10 time is preferably in the range of one minute to two hours. A preferred example of the combination of the heating temperature and the heating time is 0.1 - 1.5 hours at 180 °C and 0.1 - 1 hour at 200°C.

[0047]

15 The preferably surface cross-linking water-absorbent resin which is produced by the procedure described above is preferably adjusted to a specific particle size distribution for the sake of ensuring the effect of this invention to be satisfactorily manifested. The adjustment of the particle size distribution
20 may be performed either before or after the surface treatment. Since the water-absorbent resin of this invention possesses such an acid group as carboxyl group and/or a salt thereof, it is capable of effectively neutralizing such a basic odorous substance as ammonia, for example. It appears that the surface
25 area of the water-absorbent resin increases in proportion as the particle diameter decreases and the advantage in neutralizing the basic odorous substance increases in proportion as the surface area increases. It has been found, however, that in the actual use (for example, a gelling agent for urine as in the disposable
30 diaper), the water-absorbent resin as the gelling agent exhibits better results when it is controlled to a specific particle size distribution.

[0048]

The mechanism responsible for the manifestation of the effect of adjusting the water-absorbent resin to a specific particle size distribution remains yet to be elucidated. It is inferred, however, that the gel state of the water-absorbent resin has some bearing on the effect in question. It is inferred that then the particle size distribution is unduly small, the water-absorbent resin induces the phenomenon of gel blocking on account of an unduly high speed of absorption of fluid and the fluid which has entrained an odorous component incurs difficulty in reaching the water-absorbent resin used or the water-absorbent resin composition containing the water-absorbent resin. When the particle size distribution of the water-absorbent resin is unduly large, the odorous component is volatilized from the fluid entraining it on account of an unduly small speed of absorption of the fluid.

[0049]

To be more specific, the particles measuring not less than 150 μm and less than 850 μm preferably account for 90 mass% or more of the whole particles and the particles measuring not less than 300 μm account for 60 mass% or more of the whole particles. Preferably, the particles measuring not less than 150 μm and less than 850 μm account for not less than 95 mass% and more preferably not less than 98 mass%. The particles measuring not less than 300 μm preferably account for not less than 65 mass%, more preferably not less than 70 mass%, and particularly preferably not less than 75 mass%.

[0050]

The mass average particle diameter of the water-absorbent resin (A) is preferably in the range of 200 - 700 μm , more preferably 300 - 600 μm , and particularly preferably 400 - 500 μm . The mass average particle diameter is applied also to the

water-absorbent resin composition as described specifically herein below. The mass average particle diameter of the water-absorbent resin (A) or the water-absorbent resin composition may be adjusted, when necessary, by means of
5 granulation.

[0051]

The absorption capacity of water-absorbent resin (A) with 0.90 mass% of sodium chloride aqueous solution without load is preferably not less than 26 g/g, more preferably not less than
10 28 g/g, still more preferably not less than 30 g/g, and particularly preferably not less than 32 g/g. If the absorption capacity with 0.90 mass% of sodium chloride aqueous solution without load falls short of 26 g/g, the shortage will possibly result in preventing the effect of this invention from being
15 manifested satisfactorily.

[0052]

The absorption capacity of water-absorbent resin (A) with 0.90 mass% of sodium chloride aqueous solution under load of 1.9 kPa is preferably not less than 20 g/g, more preferably not
20 less than 22 g/g, still more preferably not less than 24 g/g, and particularly preferably not less than 26 g/g. If the absorption capacity with 0.90 mass% of sodium chloride aqueous solution under load of 1.9 kPa falls short of 20 g/g, the shortage will possibly result in preventing the effect of this invention
25 from being manifested satisfactorily.

[0053]

For the purpose of enabling the effect of this invention to be manifested to the maximum, it is particularly advantageous to use a water-absorbent resin which has not less than 26 g/g
30 of the absorption capacity with 0.90 mass% of sodium chloride aqueous solution without load and has not less than 26g/g of the absorption capacity with 0.90 mass% of sodium chloride aqueous

solution under the pressure of 1.9 kPa.

[0054]

(2) Complex oxide hydrate (B)

The complex oxide hydrate (B) is a hydrate oxide which
5 contains zinc as a main component (based on the total mass of
a metal component) and contains (b1) zinc and silicon or (b2)
zinc and aluminum. The ratio of the zinc element as a main
component in the metal component is normally
(essentially/preferably) in the range of 50 - 99.9 mass%,
10 preferably 60 - 95 mass%, and more preferably 70 - 95 mass%,
based on the total metal component. The term "water-containing
oxide," which is otherwise called a hydrated oxide, refers to
the hydrate of a metal oxide including the so-called hydroxide.
The complex oxide hydrate (B) in the case of (b1) is a
15 water-containing oxide possessing the -Zn-O-Si- bond at least
partly relative to zinc (Zn) and silicon (Si) and is different
from the mere mixture of a water-containing oxide of Zn and a
water-containing oxide of Si. By the same token, in the case
of (b2), it is a water-containing oxide possessing the -Zn-O-Al-
20 bond at least partly relative to zinc (Zn) and aluminum (Al)
and is different from the mere mixture of water-containing oxide
of Zn and water-containing oxide of Al. That is, the complex
oxide hydrate (B) contains (b1) zinc and silicon or (b2) zinc
and aluminum. For example, zeolite, the simple mixture of zinc
25 oxide and silicon dioxide, and the simple mixture of zinc oxide
and aluminum oxide are not included in the concept of the complex
oxide hydrate (B). These compounds have low zinc ratio, and
these compounds are liable to exfoliate from the surface of a
water-absorbent resin (the separation ratio described below
30 increases). They do not lend themselves to the manifestation
of the effect of this invention since zinc and silicon of the
metal components or zinc and aluminum of the metal components

don't exist close.

[0055]

When the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is present in the surface
5 of the water-absorbent resin, the gel which the water-absorbent resin forms by absorbing an aqueous fluid does not easily separate (exfoliate) from the surface of the water-absorbent resin. This behavior may be ascribable probably to the fact that the complex oxide hydrate of this invention which contains (b1) zinc and
10 silicon or (b2) zinc and aluminum has a high mass ratio of zinc content in the metal component. In the case of a complex oxide hydrate containing titanium and aluminum or titanium silicon as cited, for example, in a comparative example described specifically herein below, when the water-absorbent resin is
15 gelled by absorbing an aqueous fluid, the gel is easily separated (exfoliated) from the surface of the water-absorbent resin. In the actual application of the water-absorbent resin to a disposable diaper, for example, for the sake of heightening the deodorizing effect, the separation (exfoliation) of the gel from
20 the surface of the water-absorbent resin is preferred to be as small as permissible.

[0056]

Further, the complex oxide hydrate (B) which contains (b1) zinc and silicon or (b2) zinc and aluminum is more effective
25 than the simple mixture of the oxides of the relevant metal elements. It is inferred that since the different metals of zinc and silicon or zinc and aluminum are present in close mutual proximity, the complex oxide hydrate (B) is enabled to repress its separation from the swelled gal and exalt the deodorizing
30 effect more effectively than the mere mixture of the oxides of the relevant metal elements. When the water-absorbent resin composition of this invention is obtained by mixing the

water-absorbent resin in a powdery form and the complex oxide hydrate in a powdery form, the complex oxide hydrate uniformly adheres to the surface of the water-absorbent resin and represses conspicuously such separation as is observed in the simple
5 mixture.

[0057]

When the complex oxide hydrate (B) contains (b1) zinc and silicon or (b2) zinc and aluminum at a mass ratio contemplated by this invention as described specifically herein below, it
10 may contain other metal component. From the viewpoint of enhancing the effect further and in terms of the expense, however, the complex oxide hydrate (B) is preferred to be formed solely of the two kinds of metal, i.e. (b1) zinc and silicon or (b2) zinc and aluminum. When the complex oxide hydrate (B) has three
15 or more metal components, the content of the third metal component is preferred to be not more than 5 mass%, more preferably not more than 3 mass%, and still more preferably not more than 1 mass%, based on the total metal components. When zinc is an essential main component in the metal components, the complex
20 oxide hydrate (B) may contain magnesium, calcium, silver, copper, nickel, iron, manganese, titanium, barium, and zirconium.

[0058]

The mass ratio of the content of zinc and the content of silicon in the complex oxide hydrate (B) containing (b1) zinc
25 and silicon is preferred to be in the range of 50/50 - 99/1, more preferably 60/40 - 99/1, still more preferably 65/35 - 95/5, and particularly preferably 70/30 - 95/5. If the mass ratio deviates from the range mentioned above, the deviation will possibly result in preventing the effect of this invention to
30 be manifested satisfactorily.

[0059]

The mass ratio of the content of zinc and the content of

aluminum in the complex oxide hydrate (B) containing (b2) zinc and aluminum is preferred to be in the range of 50/50 - 99/1, more preferably 60/40 - 99/1, still more preferably 65/35 - 95/5, and particularly preferably 70/30 - 95/5. If the mass ratio
5 deviates from the range mentioned above, the deviation will possibly result in preventing the effect of this invention to be manifested satisfactorily.

[0060]

When the mass ratio of the contents of the metal components
10 in the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is not known, it may be measured by such methods as fluorescent X-ray analysis and elementary analysis, for example.

[0061]

15 The complex oxide hydrate (B) which contains (b1) zinc and silicon or (b2) zinc and aluminum is allowed to contain oxygen as a main component (based on the total mass of nonmetallic components). Hydrogen may be included in other nonmetallic components. Impure components (the by-product of reaction) may
20 be contained in a trace quantity. The ratio of the oxygen element as the main component in the nonmetallic components is generally (essentially/preferably) in the range of 50 mass% - 99.9 mass%, preferably 60 - 95 mass%, and more preferably 70 - 95 mass% in the total metal element components.

25 [0062]

The content of the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is preferably in the range of 0.001 - 5 parts by weight, more preferably 0.05 - 4 parts by weight, and still more preferably 0.1 - 3 parts
30 by weight, based on 100 parts by weight of the water-absorbent resin (A). If the content falls short of 0.001 parts by weight, the shortage will possibly result in preventing the deodorizing

property from being manifested satisfactorily. If this content exceeds 5 parts by weight, the excess will possibly result in degrading the absorbent property inherent in the water-absorbent resin.

5 [0063]

The particle diameter of the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is preferably in the range of 0.001 - 1000 μm , and more preferably 0.01 - 600 μm . The mass average particle diameter is preferably
10 not more than 500 μm and more preferably not more than 300 μm .

[0064]

The complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is preferred to be obtained by a specific method. Although the complex oxide hydrate (B)
15 containing (b1) zinc and silicon or (b2) zinc and aluminum can be obtained by various methods such as liquid phase method, gas phase method, and solid phase method, from the viewpoint of the equipment and the cost of production, it is manufactured preferably by a liquid phase method and more preferably by a
20 co-precipitation method. Generally, the term "co-precipitation method" means a procedure of causing two or more species of ions to precipitate simultaneously. In this invention, the co-precipitate of a prescribed composition is obtained by the co-precipitation method, i.e. by varying the
25 concentration, pH, temperature, and solvent of the mixed solution containing two or more species of ions thereby inducing simultaneous co-precipitation of the two or more species of ions. Then, by separating the co-precipitate and drying, the target compound is obtained. The co-precipitation method differs from
30 the method which comprises forming precipitates separately of individual metals, separating the precipitates, drying the separated precipitates thereby obtaining powders respectively,

and simply mixing the powders.

[0065]

In the production of the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum by the co-precipitation method, the method for inducing the co-precipitation does not need to be particularly restricted but may be selected from among various methods which are available. A method which comprises adding aqueous ammonia and urea to the mixed solution containing a salt of zinc and a salt of silicon or the mixed solution containing a salt of zinc and a salt of aluminum and optionally heating the resultant mixture; and a method which comprises adding an aqueous ammonia and urea to the mixed solution containing a salt of zinc and a salt of aluminum and optionally heating the resultant mixture may be cited as concrete examples of the method.

[0066]

The examples of the salts of zinc, the salts of silicon, and the salts of aluminum are not particularly restricted. The sulfates, oxysulfates, chlorides, oxychlorides, nitrates, oxynitrates, and carboxylates of zinc, silicon, and aluminum may be cited as concrete examples. Among these salts cited above, sulfates, oxysulfates, chlorides, and oxychlorides are used particularly advantageously.

[0067]

As a means to initiate the precipitation, a method for inducing co-precipitation by simultaneous hydrolysis from a mixed solution containing an alkoxide of zinc and an alkoxide of silicon; and a method for inducing co-precipitation by simultaneous hydrolysis from a mixed solution containing an alkoxide of zinc and an alkoxide of aluminum are advantageously used besides a method which uses a salt as a raw material. The examples of alkoxide of zinc, alkoxide of silicon, and alkoxide

of aluminum are not particularly discriminated. Methoxides, ethoxides, propoxides, and butoxides of zinc, silicon, and aluminum may be cited as concrete examples.

[0068]

5 The precipitating conditions during the initiation of co-precipitation are important in exerting an influence on the speed of precipitation and the shape of a co-precipitate to be produced. Since they are varied by the composition and concentration of the mixed solution, the kind of a precipitating
10 substance, the method for initiating the precipitation, and the like, they ought to be properly selected to suit such factors.

[0069]

The co-precipitate which is formed by the co-precipitation is optionally filtered, washed, and then dried. The drying
15 temperature used in this case is preferred to be comparatively low. It is preferred to be in the range of 100°C - 200°C. If the drying temperature exceeds 600°C, this unduly high temperature will possibly result in degrading the deodorizing property of the product.

20 [0070]

(3) Plant component (C)

As the plant component (C), at least one compound selected from the group consisting of polyphenols, flavones and the likes thereof, and caffeines, is contained in a proportion exceeding
25 0 and not exceeding 100 mass% based on the total mass of the plant component (C). Preferably, at least one compound selected from among tannins, tannic acid, gall, nutgall, and gallic acid is used as the plant component (C).

[0071]

30 As concrete examples of the plants containing the plant component (C), the theaceous plants such as camellia, eurya, and termstroemia, the gramineae plants such as rice, bamboograss,

bamboo, corn, and wheat, and the plants of family rubiaceae such as coffee may be cited.

[0072]

5 As concrete examples of the form of the plant component (C), the extracts (essential oil) drawn from plants, the plants themselves (plant powder), and plants lees and extraction lees by-produced during the production processes in the plant processing industry and the food processing industry may be cited, though not exclusively.

10 [0073]

The amount of the plant component (C) to be used is variable with the deodorizing function aimed at. It is preferably in the range of 0.001 - 10 parts by weight and more preferably 0.01 - 5 parts by weight based on 100 parts by weight of the water-absorbent resin (A). If this amount falls short of 0.001 parts by weight, the shortage will possibly result in preventing the effect from being satisfactorily manifested. If the amount exceeds 10 parts by weight, the excess will possibly fail to bring proportionate addition to the effect.

20 [0074]

When the plant component (C) is in the form of a powder solely; and/or when the plant component (C) is in the form of a powder having deposited thereon an extract (essential oil) drawn from a plant and containing a plant component (C); and/or
25 when the plant component (C) is in the form of a powder having an extract (essential oil) drawn from a plant and containing a plant component (C) deposited on an impalpable powder (B) formed of an aggregate of a metal hydrate oxide containing zinc and silicon or zinc and aluminum, the particle diameters of not less
30 than 90 mass% of the particles are preferably in the range of 0.001 - 1000 μm and more preferably 0.01 - 600 μm . The mass average particle diameters are preferably not more than 500 μm

and more preferably not more than 300 μm . If the mass average particle diameters exceed 500 μm , the excess will possibly render impartation of a stable deodorizing property impossible because the particles, on contacting urine, prevent the effective component contained in the plant component (C) from functioning satisfactorily. The fact that the mass average particle diameter of the powder containing the plant component (C) is smaller than the mass average particle diameter of the water-absorbent resin is at an advantage in being able to impart good deodorizing property and stability to the water-absorbent resin.

[0075]

The plant component (C) is preferred to be a liquid and/or an aqueous solution at room temperature.

[0076]

15 (4) Water-absorbent resin composition

The water-absorbent resin composition of this invention comprises the aforementioned water-absorbent resin (A) and the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum. That is, the water-absorbent resin composition of this invention is a water-absorbent resin composition which contains a water-absorbent resin (A) obtained by polymerizing an unsaturated monomer containing an acid group and/or a salt thereof as main component and a complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum.

25 [0077]

The mass ratio of the contents of zinc and silicon or the mass ratio of the contents of zinc and aluminum in the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is preferably in the range of 50/50 - 99/1, more preferably 60/40 - 99/1, still more preferably 65/35 - 90/10, and particularly preferably 70/30 - 90/10. When the mass ratio of zinc to silicone or the mass ratio of zinc to aluminum is

in the range of 1/99 - 49/52 in the complex oxide hydrate (B) containing zinc and silicon or zinc and aluminum, the deodorizing property capable of removing satisfactorily the offensive odor originating such a sulfur type compound as hydrogen sulfide and mercaptans cannot be manifested.

[0078]

The method for producing the water-absorbent resin composition is not particularly restricted. The method preferably comprises the steps of polymerizing an unsaturated monomer containing an acid group thereby obtaining a water-absorbent resin (A); and mixing the water-absorbent resin and a complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum. By this method, a water-absorbent resin composition having not less than 20 g/g of absorption capacity (value at 60 minutes) toward 0.90 mass% of sodium chloride aqueous solution under the pressure of 1.9 kPa can be obtained.

[0079]

The expression "the water-absorbent resin" (A), which can be obtained via a polymerizing step, means a water-absorbent resin which has completed undergoing a polymerization step. It embraces a water-absorbent resin which is obtained by polymerization and not given a surface cross-linking treatment and a water-absorbent resin which is given a surface cross-linking treatment after polymerization.

[0080]

The polymerizing step of polymerizing a monomer component having an acid group-containing unsaturated monomer as a main component and consequently obtaining a water-absorbent resin (A) has been already described.

[0081]

The absorption capacity of the water-absorbent resin (A) obtained via the polymerizing step toward 0.90 mass% of sodium

chloride aqueous solution without load is preferred to be not less than 26 g/g, more preferably not less than 28 g/g, still more preferably not less than 30 g/g, and particularly preferably not less than 32 g/g. If the absorption capacity toward the
5 0.90 mass% sodium chloride aqueous solution without load falls short of 26 g/g, the shortage will possibly result in preventing the effect of this invention from being manifested satisfactorily.

[0082]

The absorption capacity of the water-absorbent resin (A)
10 obtained via the polymerizing step toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa is preferably not less than 20 g/g, more preferably not less than 24 g/g, still more preferably not less than 26 g/g, and particularly preferably not less than 28 g/g. If the absorption
15 capacity toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa falls short of 20 g/g, the shortage will possibly prevent the effect of this invention to be satisfactorily manifested.

[0083]

20 For the sake of enabling the effect of this invention to be manifested to the maximum, the water-absorbent resin (A) obtained via the polymerizing step particularly preferably has an absorption capacity of not less than 26 g/g toward the 0.90 mass% sodium chloride aqueous solution without load and an
25 absorption capacity of not less than 20 g/g toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa.

[0084]

The complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is preferred to be added to
30 the water-absorbent resin (A) which has been obtained via the polymerizing step. Owing to the addition of the complex oxide hydrate (B) to the water-absorbent resin (A) obtained via the

polymerizing step, the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum is made to occur dominantly on the surface of the water-absorbent resin (A) and the effect of this invention is consequently manifested more satisfactorily. Though the manner of adding the complex oxide hydrate (B) to the water-absorbent resin obtained via the polymerizing step does not need to be particularly discriminated, the embodiment of making the addition after polymerization and drying, the embodiment of performing the addition during the course of the surface cross-linking treatment, and the embodiment of effecting the addition during the course of granulation may be cited as concrete examples of the addition. Incidentally, the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum may be added not only to the water-absorbent resin (A) obtained subsequent to polymerization but also to the monomer component prior to polymerization and to the reactants during the course of the polymerization.

[0085]

The amount of the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum to be added is preferably in the range of 0.001 - 5 parts by weight, more preferably 0.05 - 4 parts by weight, and still more preferably 0.1 - 3 parts by weight based on 100 parts by weight of the water-absorbent resin (A). If the amount of this addition falls short of 0.001 parts by weight, the shortage will possibly render deficient the deodorizing property of removing the offensive odor arising from such sulfur type compounds as hydrogen sulfide and mercaptans. If the amount exceeds 5 parts by weight, the excess will possibly result in degrading the absorbent property inherent in the water-absorbent resin.

[0086]

As concrete examples of the procedure of the addition of

the complex oxide hydrate (B) to the water-absorbent resin (A) obtained via the polymerizing step, a method of directly mixing the complex oxide hydrate (B) with the water-absorbent resin so as to ensure addition in a prescribed amount (the dry blend
5 method when the two components are both powders); a method of mixing water, an aqueous liquid, or a various organic solvent by spraying or dropwise addition with what is obtained by directly mixing into the water-absorbent resin by the method just mentioned; and a method of dispersing such additives in an aqueous
10 liquid or a various organic solvent thereby forming a slurry and adding the slurry to the water-absorbent resin may be cited. When the additives are mixed with the aqueous liquid or various organic solvent, the resultant mixture may be dried as occasion demands.

15 [0087]

When the water-absorbent resin and the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum are mixed, the optimum amount of water, steam, an aqueous solution of a hydrophilic organic solvent, or a various organic solvent
20 to be optionally added is variable with the kind and the particle size distribution of the water-absorbent resin (A). When water is used, the optimum amount of addition is preferably not more than 10 mass% and more preferably falling in the range of 1 - 5 mass%, based on the mass of the water-absorbent resin (A).
25 When a hydrophilic organic solvent is used, the amount of addition is preferably not more than 10 mass% and more preferably falling in the range of 0.1 - 5 mass%, based on the mass of the water-absorbent resin (A).

[0088]

30 The device to be used when the water-absorbent resin and the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum are mixed may be any of the various

ordinary devices available for the purpose of mixture. As concrete examples of the device, cylindrical mixers, screw type mixers, screw type extruders, high-speed stirrer type mixers (for example, turbulizers), Nautar type mixer, V shaped mixers, 5 ribbon type mixers, twin-arm type kneaders, fluid type mixers, pneumatic conveyor mixers, rotary disc type mixers, roll mixers, rolling type mixers, and spade-shaped shovel vane mixers (for example, Redige mixer) may be cited. The speed of this mixing may be high or low.

10 [0089]

The method of producing the water-absorbent resin composition of this invention may additionally incorporate therein a step of adding deodorant, antibacterial agent, perfume, foaming agent, pigment, dye, plasticizer, tackifier, surfactant, 15 fertilizer, oxidizing agent, reducing agent, water, salt, chelating agent, fungicide, hydrophilic polymer such as polyethylene glycol or polyethylene imine, hydrophobic polymer such as paraffin, thermoplastic resin such as polyethylene or polypropylene, and thermosetting resin such as polyester resin 20 or urea resin. These additives are added in a proportion preferably in the range of 0 - 30 mass%, more preferably 0 - 20 mass%, and still more preferably 0 - 10 mass% based on the mass of the water-absorbent resin.

[0090]

25 The content of the water-absorbent resin in the water-absorbent resin composition is not particularly restricted. For the sake of ensuring the effect of this invention to be satisfactorily manifested, the content is preferably in the range of 70 - 99 mass%, more preferably 80 - 99 mass%, and particularly 30 preferably 90 - 99 mass%.

[0091]

The absorption capacity of the water-absorbent resin

composition of this invention toward the 0.90 mass% sodium chloride aqueous solution without load is preferably not less than 26 g/g, more preferably not less than 28 g/g, still more preferably not less than 30 g/g, and particularly preferably
5 not less than 32 g/g. If the absorption capacity toward the 0.90 mass% sodium chloride aqueous solution without load falls short of 26 g/g, the shortage will possibly prevent the effect of this invention from being satisfactorily manifested.

[0092]

10 The absorption capacity of the water-absorbent resin composition of this invention toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa is preferably not less than 20 g/g, more preferably not less than 24 g/g, still more preferably not less than 26 g/g, and
15 particularly preferably not less than 28 g/g. If the absorption capacity toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa falls short of 20 g/g, the shortage will possibly prevent the effect of this invention from being satisfactorily manifested.

20 [0093]

For the sake of enabling the effect of this invention to be manifested to the maximum, it is particularly preferable that the water-absorbent resin composition of this invention possesses not less than 26 g/g of an absorption capacity toward
25 the 0.90 mass% sodium chloride aqueous solution without load and not less than 20 g/g of an absorption capacity toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa. Owing to the possession of such a specific excellent absorption property by the water-absorbent resin composition
30 of this invention, the deodorizing ability which is one of the effects of this invention can be manifested more satisfactorily.

[0094]

The shape of the water-absorbent resin composition is not particularly restricted. Spheres, an aggregate of beads, and an amorphously crushed powder (particles) may be cited as concrete examples of the shape. In view of the height of the fixing property to fibers, the amorphously crushed powder (particles) is preferably adopted. For the sake of ensuring the effect of this invention to be satisfactorily manifested, the bulk density specified in JIS K-3362 is preferably in the range of 0.40 - 0.80 g/ml, more preferably 0.50 - 0.75 g/ml, and more preferably 0.60 - 0.73 g/ml.

[0095]

The water content of the water-absorbent resin composition is not particularly restricted (the water content is specified as the amount of water contained in the water-absorbent resin composition. For example, it is calculated by using 1 g of a given water-absorbent resin and finding the amount lost by three hours' drying at 180°C). For the sake of ensuring the effect of this invention to be satisfactorily manifested, the water-absorbent resin composition is preferred to be a powder which exhibits fluidity even at room temperature. To be specific, the water content is preferably in the range of 0.2 - 30 mass%, more preferably 0.3 - 15 mass%, and still more preferably 0.5 - 10 mass%.

[0096]

The amount of the water-soluble component of the water-absorbent resin composition is not particularly restricted, but the value is preferred to be lower. For the sake of ensuring the effect of this invention to be satisfactorily manifested, it is preferred to be not more than 50 mass%, more preferably not more than 25 mass%, still more preferably not more than 20 mass%, particularly preferably not more than 15 mass%, and most preferably not more than 10 mass%.

[0097]

The degree of discoloration of the water-absorbent resin composition, as expressed by the YI index (Yellow Index: refer to European Patent No. 942014 and European Patent No. 1108745), is preferably in the range of 0 - 15, more preferably 0 - 13, still more preferably 0 - 10, and most preferably 0 - 5. The amount of the residual monomer in the water-absorbent resin composition is preferably not more than 1000 ppm and more preferably not more than 500 ppm.

10 [0098]

As regards the particle size distribution of the water-absorbent resin composition, preferably the particles measuring less than 850 μm and not less than 150 μm account for not less than 90 mass% of all the particles and the particles measuring not less than 300 μm account for not less than 60 mass% of all the particles. Preferably, the particles measuring less than 850 μm and not less than 150 μm is concluded more. Specifically, the particles measuring less than 850 μm and not less than 150 μm account for preferably 95 - 100 mass% and more preferably 98 - 100 mass% of all the particles. Then, the particles measuring not less than 300 μm account for preferably not less than 65 mass%, more preferably not less than 70 mass%, and particularly preferably not less than 75 mass% of all the particles. [0099]

25 If the particles measuring not less than 300 μm account for less than 60 mass%, the shortage will possibly render the accomplishment of the deodorizing effect of this invention difficult. In spite of the fact that the surface area to be covered decreases in proportion as the particle diameter is increased, the deodorizing effect is enhanced incredibly in accordance as the particle diameter of the water-absorbent resin composition is enlarged and the specific surface area thereof

30

is decreased.

[0100]

The mass average particle diameter of the water-absorbent resin composition is preferably in the range of 200 - 700 μm ,
5 more preferably 300 - 600 μm , and particularly preferably 400 - 500 μm . The mass average particle diameter of the water-absorbent resin composition may be optionally adjusted by means of granulation, for example.

[0101]

10 For the sake of enabling the water-absorbent resin composition to acquire a good deodorizing property, the amount of the hydrogen sulfide residue under wet after three hours is preferably not more than 5 ppm, more preferably not more than 3 ppm, still more preferably not more than 2 ppm, and particularly
15 preferably not more than 1 ppm. Further, the amount of the hydrogen sulfide residue under wet after one hour is preferably not more than 7 ppm, more preferably not more than 5 ppm, and particularly preferably not more than 3 ppm. The amount of the hydrogen sulfide residue under wet after 30 minutes is preferably
20 not more than 9 ppm, more preferably not more than 7 ppm, and particularly preferably not more than 5 ppm.

[0102]

For the sake of enabling the water-absorbent resin composition of this invention to acquire a good deodorizing
25 property, the amount of wet ammonia residue after 60 minutes is preferably not more than 50 ppm, more preferably not more than 40 ppm, and particularly preferably not more than 30 ppm. The amount of wet ammonia residue after 30 minutes is preferably not more than 100 ppm, more preferably not more than 80 ppm,
30 and particularly preferably not more than 60 ppm. Further, the amount of wet ammonia residue after 10 minutes is preferably not more than 300 ppm, more preferably not more than 250 ppm,

and particularly preferably not more than 220 ppm. The water-absorbent resin composition effectively manifests the deodorizing property because the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum possesses a low separation ratio (for details of the separation ratio, refer to the example section cited herein below). The separation ratio of the complex oxide hydrate (B) containing zinc and silicon or zinc and aluminum is preferred to be lower. Specifically, the separation ratio of the complex oxide hydrate (B) is preferably not more than 20%, more preferably not more than 15%, still more preferably not more than 10%, and particularly preferably not more than 5%. If the separation ratio of the complex oxide hydrate (B) containing zinc and silicon or zinc and aluminum exceeds 20%, the excess will possibly prevent the deodorizing effect possessed by the complex oxide hydrate (B) containing zinc and silicon or zinc and aluminum from being manifested effectively because the water-absorbent resin and the complex oxide hydrate (B) containing zinc and silicon or zinc and aluminum are separated when the water-absorbent resin composition is swelled by absorbing a fluid such as urine.

[0103]

The water-absorbent resin composition excels in the powder handling property because it has a low hygroscopic blocking ratio as described in the example section cited herein below. The hygroscopic blocking ratio is preferred to be lower. Specifically, the hygroscopic blocking ratio is preferably not more than 30 mass%, more preferably not more than 20 mass%, still more preferably not more than 10 mass%, and particularly preferably not more than 5 mass%. If the hygroscopic blocking ratio exceeds 30 mass%, the excess will possibly entail such disadvantages as impairing the fluidity of powder during the production of disposable diaper, for example, and rendering the

production of the disposable diaper difficult.

[0104]

(5) Absorbent material

The water-absorbent resin composition of this invention
5 has the water-absorbent resin (A) as a main component and generally
assumes the form of powder. The absorbent material is obtained
by causing the powdery water-absorbent resin composition to be
formed in conjunction with other arbitrary absorbent material.
The shape of the absorbent material is not particularly restricted.
10 Preferred shapes thereof include sheets (otherwise called webs),
cylinders, films, and fibers. The absorbent material is
particularly preferred to be in the shape of sheet. When the
water-absorbent resin composition is obtained in the shape of
a sheet, the sheet may be used directly as an absorbent material.

15 [0105]

For the sake of manifesting the effect of this invention,
the absorbent material contains the water-absorbent resin (A)
possessing a cross-linked structure with an acid group and/or
a salt thereof as a main component and contains the complex oxide
20 hydrate (B) containing (b1) zinc and silicon or (b2) zinc and
aluminum and hydrophilic fibers.

[0106]

The hydrophilic fibers are not particularly restricted.
As concrete examples of the hydrophilic fibers, ground wood pulp,
25 cotton linters, cross-linked cellulose fibers, rayon, cotton,
wool, acetate, and vinylon™ may be cited. Preferably, products
obtained by air-laiding these materials are used.

[0107]

The absorbent material of this invention may be produced
30 by using the water-absorbent resin composition described above
and the hydrophilic fibers. It may be otherwise produced by
using the water-absorbent resin (A) possessing the cross-linked

structure with an acid group and/or a salt thereof, the complex oxide hydrate (B) containing (b1) zinc and silicon or (b2) zinc and aluminum, and the hydrophilic fibers.

[0108]

5 When the absorbent material of this invention is an absorbent material which contains the water-absorbent resin composition and the hydrophilic fibers, the content of the water-absorbent resin composition based on the total mass of the water-absorbent resin composition and the hydrophilic fibers (the core
10 concentration) preferably falls in the range of 20 - 100 mass%, more preferably 25 - 90 mass%, and still more preferably 30 - 80 mass%. If the core concentration falls short of 20 mass%, the amount of the water-absorbent resin composition to be used is small, and the shortage will possibly render insufficient
15 the impartation of the deodorizing property to the entire disposable diaper, for example.

[0109]

When the absorbent material of this invention is produced from the water-absorbent resin composition and the hydrophilic
20 fibers, the method for effecting this production is not particularly restricted. The absorbent material is produced, for example, by dry-mixing the water-absorbent resin composition and the hydrophilic fibers in a ratio calculated to fall in the range of the core concentration mentioned above by the use of
25 a mixing device such as a mixer, forming the resultant mixture in the shape of a web by means of pneumatic webbing, and, if necessary, subsequently subjecting the web to compression molding. This absorbent material is preferred to be compressed to a density in the range of 0.001 - 0.50 g/cm³ and a basis weight
30 in the range of 0.01 - 0.20 g/cm².

[0110]

When the absorbent material of this invention is produced

by using the water-absorbent resin (A) or the water-absorbent resin composition, the complex oxide hydrate (B), and the hydrophilic fibers, the absorption capacity of the water-absorbent resin (A) toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa is preferred to be not less than 20 g/g. The mass ratio of zinc and silicon or zinc and aluminum in the complex oxide hydrate (B) is preferred to be in the range of 50/50 - 99/1. Further, the absorption capacity (value at 60 minutes) of the water-absorbent resin toward the 0.90 mass% sodium chloride aqueous solution under the pressure of 1.9 kPa is preferred to be in the aforementioned range. If the mass ratio of zinc and silicon or zinc and aluminum in the complex oxide hydrate (B) deviates from the range mentioned above, the deviation will possibly prevent the absorbent material from manifesting the effect of this invention sufficiently.

[0111]

When the absorbing material of this invention is produced by using the water-absorbent resin (A), the complex oxide hydrate (B), and the hydrophilic fibers, the method for production is not particularly restricted. For example, a method of dry-mixing the water-absorbent resin, the complex oxide hydrate (B) including (b1) zinc and silicon or (b2) zinc and aluminum, and the hydrophilic fibers at a ratio calculated to form the core concentration mentioned above by the use of a mixing device such as a mixer; a method of having water, aqueous liquid, and various organic solvent mixed by spraying or dropwise addition with the product of the dry-mixing; and a method of mixing a slurry resulting from dispersing the complex oxide hydrate (B) in an aqueous liquid or a various organic solvent with the water-absorbent resin and the hydrophilic fibers at a ratio calculated to form the core concentration mentioned above by the use of a mixing device such as a mixer may be cited as concrete

examples of the method available for the production.

[0112]

(6) Absorbent product

The absorbent product of this invention is furnished with
5 the absorbent material of this invention described above, a
liquid-permeable topsheet, and a liquid-impermeable backsheet.

[0113]

The method of producing the absorbent product is not
particularly restricted. The absorbent material is interposed
10 between a liquid-permeable medium (the topsheet) and a liquid
impermeable medium (the backsheet). By optionally disposing
an elastic member, a dispersing layer, and an adhesive tape,
an absorbent product such as, for example, an adult disposable
diaper or a sanitary napkin is produced.

15 [0114]

The water-absorbent resin composition and the absorbent
material of this invention can impart a deodorizing function
to the absorbent product and continue to exhibit excellent
deodorizing property and absorbent property for a long time.
20 As concrete use, such sanitary material as adult disposable diaper,
infant disposable diaper, sanitary napkin, and so-called
incontinence pad may be cited, though not exclusively. The
absorbent product of this invention enjoys the veritably
outstanding deodorizing ability inherent in the water-absorbent
25 resin composition and the absorbent material, prevents the re-wet
of fluid significantly, and emits a conspicuous dry sensation.
Further, it greatly alleviates the burden on the person wearing
the product and on the person nursing the person using it.

[Example]

30 [0115]

Now, examples and comparative examples of this invention
will be specifically explained below. This invention is not

limited to the following examples. Incidentally, the various properties of the water-absorbent resin, water-absorbent resin composition, and absorbent product indicated herein below were determined by the following methods. All the electrical devices used in the examples were invariably operated under the conditions of 100 V and 60 Hz. Further, the water-absorbent resin, the water-absorbent resin composition, and the absorbent product were used under the conditions of $25^{\circ}\text{C} \pm 2^{\circ}\text{C}$ and RH 50% unless otherwise specified.

10 [0116]

(a) Absorption capacity toward the 0.90 mass% sodium chloride aqueous solution (physiological saline) without load

A given water-absorbent resin (or water-absorbent resin composition) weighing 0.20 g was uniformly placed in a pouch (60 mm \times 60 mm) made of non-woven fabric and immersed in an 0.9 mass% sodium chloride aqueous solution (physiological saline) adjusted to a temperature of $25 \pm 2^{\circ}\text{C}$ for 60 minutes. After the immersion, the pouch was lifted from the solution, drained with a centrifugal separator at 250 G for three minutes, and weighed to find the mass W2 (g) of the pouch. The same procedure was repeated without using the water-absorbent resin (or water-absorbent resin composition) to find the mass W1 (g) of the pouch. The absorption capacity (g/g) was calculated in accordance with the following formula using the two masses, W1 and W2 determined above.

[0117]

Absorption capacity (g/g) toward the 0.90 mass% sodium chloride aqueous solution (physiological saline) without load = $[(\text{Mass W2 (g)} - \text{mass W1 (g)}) / \text{mass (g) of the water-absorbent resin (or water-absorbent resin composition)}] - 1$

(b) Absorption capacity toward the 0.90 mass% sodium chloride aqueous solution (physiological saline) under the

pressure of 1.9 kPa

A given water-absorbent resin (or water-absorbent resin composition) weighing 0.90 g was uniformly scattered on a 400-mesh wire sheet made of stainless steel (mesh size 38 μ m) fused to the bottom cylindrical section of a plastic supporting cylinder having an inside diameter of 60 mm. A piston (cover plate) having an outside diameter of slightly smaller than 60 mm, producing no gap with the wall surface of the supporting cylinder, and offering no obstruction to its own vertical motion was mounted on the water-absorbent resin. The supporting cylinder, the water-absorbent resin (or water-absorbent resin composition), and the piston were weighed to determine the total mass W_3 (g). The whole system of determination was completed by mounting on the piston a load adjusted to exert uniformly a load of 1.9 kPa inclusive of the piston to bear on the water-absorbent resin (or water-absorbent resin composition). A glass filter 90 mm in diameter and 5 mm in thickness was placed inside a petri dish 150 mm in diameter and 0.9 mass% sodium chloride aqueous solution (physiological saline) adjusted to $25 \pm 2^\circ\text{C}$ was added to the petri dish till it rose to the same level as the upper surface of the glass filter. One sheet of filter paper 9 cm in diameter (produced by Toyo Roshi K.K. and sold under product code of "No. 2") was mounted on the glass filter and left standing thereon till the surface was completely wetted, with the excess liquid removed from the petri dish.

[0118]

The whole system of determination was mounted on the wet filter paper and the water-absorbent resin was enabled to absorb the liquid under the load. When the liquid level fell from the upper part of the glass filter, the liquid was replenished so as to retain the liquid level constant. After the elapse of one hour, the whole system of determination was lifted and the

mass W4 (g) (the total mass of the supporting cylinder, the swelled water-absorbent resin (or water-absorbent resin composition), and the piston) remaining after the removal of the load was determined. The absorption capacity (g/g) toward the 0.90 mass% sodium chloride aqueous solution (physiological saline) under the pressure of 1.9 kPa was calculated in accordance with the following formula using the masses W3 and W4 determined above.

[0119]

Absorption capacity (g/g) toward 0.90 mass% sodium chloride aqueous solution (physiological saline) under the pressure of 1.9 kPa = (Mass W4 (g) - mass W3 (g)) / mass (g) of the water-absorbent resin (or water-absorbent resin composition)

(c) Mass average particle diameter

A given water-absorbent resin or water-absorbent resin composition was passed through JIS standard sieves having apertures of 850 μm , 600 μm , 500 μm , 425 μm , 300 μm , 212 μm , 150 μm , 106 μm , and 75 μm and the residual percentages consequently found were plotted on a logarithmic probability paper. The mass average particle diameter (D50) of the water-absorbent resin was read from the paper.

[0120]

The screening was carried out by charging the JIS standard sieves having apertures of 850 μm , 600 μm , 500 μm , 425 μm , 300 μm , 212 μm , 150 μm , 106 μm , and 75 μm (the Iida Testing Sieve; inside diameter 80 mm) with a given water-absorbent resin powder or water-absorbent resin composition powder weighing 10.00 g and shaking these sieves with a low-tap type sieve shaker (made by Iida Seisakusho K.K. and sold under the trademark designation of "ES-65 Type Sieve Shaker") for 10 minutes. The term "mass average particle diameter (D50)" used herein refers to the particle diameter of the standard sieve corresponding to 50 mass% of all the particles separated by the standard sieves of fixed

apertures as described in U.S. Patent No. 5051259, for example.

[0121]

(d) Deodorizing test (rating of water-absorbent resin or water-absorbent resin composition)

5 In a lidded polypropylene cup having an inner volume of
120 ml, 50 ml of human urine collected from 20 adults was placed
and a sample weighing 2.0 g of each of the water-absorbent resin
(or water-absorbent resin compositions) obtained in the examples
and the comparative examples described herein below was placed
10 in the urine to obtain a swelled gel. The human urine used herein
was within two hours old from the time of excretion. The cup
was lidded and the swelled gel was retained therein at 37°C.
The lid was removed from the cup six hours after the absorption
of the urine. The deodorizing effect was rated by causing 20
15 adult panel members to smell the interior of the cup at a position
of about 3 cm from the upper part of the cup. For the sake of
the rating, the panel members recorded the results of sensory
test according to the following standard using a six-point scale
and the recorded points were averaged. The test was performed
20 by following the procedure while omitting the addition of
water-absorbent resin (or water-absorbent resin composition)
and using human urine alone. The product of this test was adopted
as the standard. The deodorizing effect was rated by using the
smell of this standard taken as the point 5 on the scale.

25 [0122]

0: Absence of smell.

1: Barely discernible smell.

2: Discernible yet tolerable smell.

3: Easily discernible smell.

30 4: Strong smell.

5: Intense smell.

(e) Deodorizing test (rating of absorbent product)

Each of the absorbent products obtained in the examples and the comparative examples which will be described specifically herein below was cut to separate a circle (80 mm in diameter). On the bottom of a lidded propylene cup having an inner volume of 500 ml, the circle was placed with the liquid-permeable sheet held on the upper side. In the central part of the absorbent product, 20 g of human urine collected from 20 adults was placed. The cup was lidded and was wholly retained at 37°C. The lid was removed from the cup six hours thereafter. The deodorizing effect was rated by causing 20 adult panel members to smell the interior of the cup at a position of about 3 cm from the upper part of the cup. For the sake of the rating, the panel members recorded the results of sensory test according to the following standard using a six-point scale and the recorded points were averaged. The test was performed by following the procedure while omitting the addition of absorbent product and using human urine alone. The product of this test was adopted as the standard. The deodorizing effect was rated by using the smell of this standard taken as the point 5 on the scale.

[0123]

0: Absence of smell.

1: Barely discernible smell.

2: Discernible yet tolerable smell.

3: Easily discernible smell.

4: Strong smell.

5: Intense smell.

(f) Amount of the hydrogen sulfide residue under wet (test for ability to deodorize hydrogen sulfide)

In a glass petri dish (a product measuring 150 mm in outside diameter and 28 mm in height, entered under the code 305-08 in General Catalogue A-8000 published by Sogo Rikagaku Glass Seisakusho K.K. (in 2002)), a given water-absorbent resin (or

water-absorbent resin composition) weighing 5.00 g was uniformly scattered. Then, one sheet of a gas-permeable and liquid-permeable Heatron paper (made by Nangoku Pulp Kogyo K.K. and sold under the product code of "GSP-22") cut into a circle
5 was placed to cover the water-absorbent resin (or water-absorbent resin composition), with three portions of the circumference of the paper fixed to the inner wall of the glass petri dish with adhesive tape (10 mm × 10 mm). Non-woven fabric was substituted for the paper when the Heatron paper was not available.
10 A 3L smelling bag (made by Ohmi Odo Air Service K.K.) was opened along one side to admit the glass petri dish having the water-absorbent resin (or water-absorbent resin composition) scattered thereon and then the opened part of the bag was closed so as to leave no gap behind. The smelling bag was provisionally
15 decompressed via the glass tube part furnished for the smelling bag and then made to introduce a prescribed amount of odorless air. The amount of the odorless air to be introduced was so set that the total amount of the odorless air and the standard hydrogen sulfide gas to be introduced afterward would reach 2.5
20 L. The amount was set in accordance with the formula, amount of odorless air (L) = 2.5 - amount of standard hydrogen sulfide gas to be injected (L). Subsequently, 80 ml of an 0.90 mass% sodium chloride aqueous solution (physiological saline) adjusted to a temperature of $25 \pm 2^{\circ}\text{C}$ was poured without pausing into
25 the petri dish inside the smelling bag by means of a glass funnel fitted with a teflon (trademark) tube while preventing entry of ambient air so as to induce uniform swelling of the water-absorbent resin (or water-absorbent resin composition). The smelling bag was then tightly closed with a silicon rubber
30 stopper. After the elapse of 30 minutes from the time of swelling, 1.0 ml of the standard hydrogen sulfide gas (hydrogen sulfide concentration: 5.06 (vol. %), the hydrogen sulfide concentration

in the smelling bag: 20 ppm) was injected into the smelling bag with a syringe possessing an injection needle and was left standing therein at 25°C. The standard gas concentration and the amount of injection were properly varied so as to set the concentration in the bag at 20 ppm. After the elapse of 30 minutes, one hour, and three hours, the atmospheric concentration was determined by using a gas collecting device (made by Gastech K.K. and sold under the product code of "GV-100S") and a gas sensing tube (made by Gastech K.K. and sold under the product code of No 4LK") while preventing entry of ambient air. This atmospheric concentration was reported as the amount of the hydrogen sulfide residue under wet.

[0124]

(g) Amount of wet ammonia residue

In a glass petri dish (a product measuring 150 mm in outside diameter and 28 mm in height, entered under the code 305-08 in General Catalogue A-8000 published by Sogo Rikagaku Glass Seisakusho K.K. (in 2002), a given water-absorbent resin (or water-absorbent resin composition) weighing 5.00 g was uniformly scattered. Then, one sheet of a gas-permeable and liquid-permeable Heatron paper (made by Nangoku Pulp Kogyo K.K. and sold under the product code of "GSP-22") cut into a cycle was placed to cover the water-absorbent resin (or water-absorbent resin composition), with three portions of the circumference of the paper fixed to the inner wall of the glass petri dish with adhesive tape (10 mm × 10 mm). Non-woven fabric was substituted for the paper when the Heatron paper was not available. A 3L smelling bag (made by Ohmi Odo Air Service K.K.) was opened along one side to admit the glass petri dish having the water-absorbent resin (or water-absorbent resin composition) scattered thereon and then the opened part of the bag was closed so as to leave no gap behind. The smelling bag was provisionally

decompressed via the glass tube part furnished for the smelling bag and then made to introduce a prescribed amount, i.e. 2.5 L, of odorless air. Subsequently, 80 ml of an 0.90 mass% sodium chloride aqueous solution (physiological saline) having the temperature adjusted to $25 \pm 2^\circ\text{C}$ and having 0.0132 mol of ammonia dissolved therein was poured without pausing into the petri dish inside the smelling bag by means of a glass funnel fitted with a polytetrafluoroethylene tube while preventing entry of ambient air so as to induce uniform swelling of the water-absorbent resin (or water-absorbent resin composition). The smelling bag was then tightly closed with a silicon rubber stopper and left standing at 25°C . After the elapse of 10 minutes, 30 minutes, and 60 minutes, the silicon rubber stopper was removed and the atmospheric concentration was determined by using a gas collecting device (made by Gastech K.K. and sold under the product code of "GV-100S") and a gas sensing tube (made by Gastech K.K. and sold under the product code of "No 3L, No. 3La, No. 3M") while preventing entry of ambient air. This atmospheric concentration was reported as the amount of wet ammonia residue.

[0125]

(h) Separation ratio (the index showing the proportion of the additives to the water-absorbent resin exfoliated from the water-absorbent resin in a swollen state)

An Erlenmeyer flask made of clear glass and having an inner volume of 200 ml (made by Sogo Rikagaku Glass Seisakusho K.K.) was packed with 0.50 parts by weight of a water-absorbent resin composition and 50 ml of 0.90 mass% sodium chloride aqueous solution (physiological saline) adjusted to a temperature of $25 \pm 2^\circ\text{C}$. Then, a stirrer (the standard type measuring 3 cm in length, made by Sogo Rikagaku Glass Seisakusho K.K.) was placed in the flask, and the flask was tightly closed with a silicon rubber stopper, and the content was stirred with a magnetic stirrer

at 300 rpm for 10 minutes. After completion of the stirring, the flask was disposed in an ultrasonic cleaner (made by Shinnissei Denshi K.K., distributed by K.K. Baliba, and sold under the trademark designation of "Ultra-Sonic Cleaner 7500 Baliba").

5 Purified water was poured into the bath of the ultrasonic cleaner till it rose to the same height as the liquid level inside the flask. Then, the ultrasonic cleaner was operated for 20 minutes. Thereafter, the whole liquid in the flask was stirred again at 300 rpm for one minute so as to homogenize the liquid. Immediately

10 after the elapse of this one minute, the content of the flask was subjected to filtration under reduced pressure (using a filter paper made by Advantec K.K. and sold under the product code of "No. 2"). The filtrate was wholly recovered and weighed to determine the mass W5 (g) thereof. The filtrate consequently

15 obtained was tested for haze value by means of a digital haze meter (made by Nippon Denshoku Kogyo K.K. and sold under the trademark designation of "Automatic Digital Hazemeter NDH-20D"). The kaoline turbidity was calculated from the relation between the haze value and the kaoline turbidity. Further, from the

20 calibration curve obtained by the method which will be specifically described herein below, the concentration X1 (ppm) of the additives in the filtrate, namely, the amount of the additives separated from the water-absorbent resin into the 0.90 mass% sodium chloride aqueous solution (physiological saline),

25 was calculated.

[0126]

The calibration curve described by the amounts of the individual additives and the kaoline turbidity was formed as follows. In an Erlenmeyer flask made of clear glass and having

30 an inner volume of 200 ml (made by Sogo Rikagaku Glass Seisakusho K.K.), 50 ml of an 0.90 mass% sodium chloride aqueous solution (physiological saline) containing a prescribed amount

(equivalent to 20 ppm, 50 ppm, 100 ppm, and 300 ppm) of additive and adjusted to a temperature of $25 \pm 2^{\circ}\text{C}$ was prepared. Then, a stirrer (the standard type measuring 3 cm in length, made by Sogo Rikagaku Glass Seisakusho K.K.) was placed in the flask, and the flask was tightly closed with a silicon rubber stopper, and the content was stirred with a magnetic stirrer at 300 rpm for 10 minutes. After completion of the stirring, an ultrasonic cleaner (made by Shinnissei Denshi K.K., distributed by K.K. Bariba, and sold under the trademark designation of "Ultra-Sonic Cleaner 7500 baliba") was disposed in the flask. Purified water was poured into the bath of the ultrasonic cleaner till it rose to the same height as the liquid level inside the flask. Then, the ultrasonic cleaner was operated for 20 minutes. Thereafter, the whole liquid in the flask was stirred again with a magnetic stirrer at 300 rpm for one minute so as to homogenize the liquid. Immediately after the elapse of one minute, the content of the flask was subjected to filtration under reduced pressure (using a filter paper made by Advantec K.K. and sold under the product code of "No. 2"). The filtrate was wholly recovered. The filtrate consequently obtained was tested for haze value by means of a digital hazemeter (made by Nippon Denshoku Kogyo K.K. and sold under the trademark designation of "Automatic Digital Hazemeter NDH-20D"). The kaoline turbidity was calculated from the relation between the haze value and the kaoline turbidity. The relation between the known amount of additive and the kaoline turbidity was linearly approximated by the least-square method to form a calibration curve for each of the additives.

[0127]

The separation ratio was calculated in accordance with the following formula.

[0128]

$$\text{Separation ratio (\%)} = X1/Y1 \times 100$$

X1 (ppm): Concentration of additive in the filtrate calculated empirically

Y1 (ppm): Concentration of filtrate having the additive wholly separated from the water-absorbent resin and dispersed in the filtrate

$$Y1 \text{ (ppm)} = 0.50 \times A1/100/W5 \times 1000000$$

A1 (mass%): Amount of additive used (toward the water-absorbent resin)

W5 (g): Amount of filtrate

The formula indicates that the exfoliation of the additive from the water-absorbent resin decreases and the effect of the additive to be manifested gains in magnitude in accordance as the value of the separation ratio decreases.

(i) Hygroscopic blocking ratio (mass%)

A given water-absorbent resin (or water-absorbent resin composition) weighing 2 g was uniformly scattered on the bottom of an aluminum cup measuring 52 mm in diameter of the bottom surface and 22 mm in height. The cup containing the water-absorbent resin was quickly placed in a thermo-humidistat (made by Tabai Espec k.k. and sold under the trademark designation of "Platiodus Lucifer PL-2G") adjusted in advance to 25°C and RH 90% and left standing therein for 60 minutes. Then, the water-absorbent resin (or water-absorbent resin composition) which had absorbed moisture was transferred onto a JIS standard sieve measuring 7.5 cm in diameter and having an aperture of 2000 μm. When the moistened water-absorbent resin (or water-absorbent resin composition) happened to adhere strongly to the aluminum cup and defy transfer to the sieve, the water-absorbent resin (or water-absorbent resin composition) which had absorbed moisture and had undergone the phenomenon of blocking was peeled off heedfully to avoid inflicting breakage and then transferred to the sieve. The water-absorbent resin

in the sieve was immediately shaken for 8 seconds with a shaking classifier (Iida sieve shaker, Type ES-65, SER No. 0501) to determine the amount, W6 (g), of the water-absorbent resin (or water-absorbent resin composition) stopped on the sieve and the
5 amount, W7 (g), of the water-absorbent resin (or water-absorbent resin composition) passed through the sieve.

The hygroscopic blocking ratio (mass%) was calculated in accordance with the following formula. The formula indicates that the hygroscopic fluidity gained in excellence and the powder
10 handling property gained in enhancement in accordance as the hygroscopic blocking ratio decreased.

Hygroscopic blocking ratio (mass%) = $\text{Weight, } w_6 \text{ (g)} / (\text{weight } W_6 \text{ (g)} + \text{weight } W_7 \text{ (g)}) \times 100$

[0129]

15 [Referential Example 1]

A reaction solution was obtained by dissolving 3.4 g of polyethylene glycol diacrylate (the average addition mol number of ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 38 mass%) having a neutralizing ratio
20 of 75 mol%. Then, this reaction solution was deaerated under an atmosphere of nitrogen gas for 30 minutes. The reaction solution mentioned above was subsequently supplied to a reaction vessel formed by attaching a lid to a twin arm type jacketed kneader made of stainless steel, furnished with two sigma type
25 vanes, and having an inner volume of 10 L. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. When 2.46 g of sodium persulfate and 0.10 g of L-ascorbic acid were added to the reaction solution while the reaction solution was continuously kept stirred, polymerization was
30 started about one minute thereafter. Then, the polymerization was carried out at 30°C - 90°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes after the start

of the polymerization. The hydrogel polymer thus obtained was finely divided into particles 1 - 4 mm in diameters. The finely divided hydrogel polymer was spread on a 50-mesh metal sheet (having a mesh size of 300 μ m) and dried with hot air at 150°C for 90 minutes. Then, the dried particles were pulverized by the use of a shaking mill, further classified with a metal sheet having an aperture of 20 mesh (having a mesh size of 850 μ m). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (a).

10 [0130]

100 parts by weight of the water-absorbent resin powder (a) was mixed with 3.83 parts by weight of a surface cross-linking agent composed of 0.5 parts by weight of propylene glycol, 0.03 parts by weight of ethylene glycol diglycidyl ether, 0.3 parts by weight of 1,4-butane diol, and 3 parts by weight of water. A water-absorbent resin (1) was obtained by subjecting the resultant mixture to a heat treatment at 210°C for 55 minutes. The absorption capacity without load, the absorption capacity under the pressure, and the particle size distribution of this water-absorbent resin (1) are shown in Table 1.

[0131]

[Referential Example 2]

A reaction solution was formed by dissolving 5.9 g of polyethylene glycol diacrylate (average addition mol number of ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 38 mass%) having a neutralizing ratio of 65 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 2.46 g of sodium persulfate and 0.10 g of L-ascorbic

acid were added to the stirred reaction solution, polymerization was started about one minute thereafter. The polymerization was carried out at 30°C - 90°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes thereafter.

5 The hydrogel polymer thus obtained was finely divided into particles about 1 - 4 mm in diameters. This hydrogel polymer was dried and pulverized in the same manner as in Referential Example 1 and further classified with a metal sheet having an aperture of 20 mesh (mesh size 850 μm). And, the classified

10 particles were blended to obtain an amorphously pulverized water-absorbent resin powder (b).

100 parts by weight of the water-absorbent resin powder (b) thus obtained was mixed with 3.8 parts by weight of a surface cross-linking agent composed of 0.5 parts by weight of propylene glycol, 0.3 parts by weight of 1,4-butane diol, and 3 parts by weight of water. A water-absorbent resin (2) was obtained by

15 subjecting the resultant mixture to a heat treatment at 200°C for 45 minutes. The results are shown in Table 1.

[0132]

20 [Referential Example 3]

A reaction solution was formed by dissolving 3.6 g of polyethylene glycol diacrylate (average addition mol number of ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 33 mass%) having a neutralizing ratio

25 of 60 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously

30 stirred and 2.46 g of sodium persulfate and 0.10 g of L-ascorbic acid were added to the stirred reaction solution, polymerization was started about one minute thereafter. The polymerization

was carried out at 30°C - 85°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes thereafter. The hydrogel polymer thus obtained was finely divided into particles about 1 - 4 mm in diameters. This hydrogel polymer
5 was dried and pulverized in the same manner as in Referential Example 1 and further classified with a metal sheet having an aperture of 20 mesh (mesh size 850 µm). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (c).

10 100 parts by weight of the water-absorbent resin powder (c) thus obtained was mixed with 3.83 parts by weight of a surface cross-linking agent having the same composition as in Referential Example 1. A water-absorbent resin (3) was obtained by subjecting the resultant mixture to a heat treatment at 195°C
15 for 40 minutes. The results are shown in Table 1.

[0133]

[Referential Example 4]

A reaction solution was formed by dissolving 3.3 g of polyethylene glycol diacrylate (average addition mol number of
20 ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 30 mass%) having a neutralizing ratio of 55 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having
25 the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 2.46 g of sodium persulfate and 0.10 g of L-ascorbic acid were added to the stirred reaction solution, polymerization was started about one minute thereafter. The polymerization
30 was carried out at 30°C - 85°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes thereafter. The hydrogel polymer thus obtained was finely divided into

particles about 1 - 4 mm in diameters. This hydrogel polymer was dried and pulverized in the same manner as in Referential Example 1 and further classified with a metal sheet having an aperture of 20 mesh (mesh size 850 μ m). And, the classified
5 particles were blended to obtain an amorphously pulverized water-absorbent resin powder (d).

100 parts by weight of the water-absorbent resin powder (d) thus obtained was mixed with 3.8 parts by weight of a surface cross-linking agent of the same composition as in Referential
10 Example 2. A water-absorbent resin (4) was obtained by subjecting the resultant mixture to a heat treatment at 195°C for 40 minutes. The results are shown in Table 1.

[0134]

[Referential Example 5]

15 A reaction solution was formed by dissolving 5.3 g of polyethylene glycol diacrylate (average addition mol number of ethylene oxide 8) in 6600 g of sodium acrylate aqueous solution (monomer concentration 35.5 mass%) having a neutralizing ratio of 68 mol%. Then, this reaction solution was deaerated in the
20 same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 3.23 g of sodium persulfate and 0.016 g of L-ascorbic
25 acid were added to the reaction solution, polymerization was started about one minute thereafter. The polymerization was carried out at 30°C - 90°C. A polymer of the hydrogel form was extracted from the reaction vessel 40 minutes thereafter. The hydrogel polymer thus obtained was finely divided into particles
30 about 1 - 4 mm in diameters. The hydrogel polymer was spread on a metal sheet having an aperture of 50 mesh (mesh size 300 μ m) and dried with hot air at 170°C for 40 minutes. Then, the

dried particles were pulverized by the use of a shaking mill, further classified with a metal sheet having an aperture of 20 mesh (having a mesh size of 850 μ m). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (e).

100 parts by weight of the water-absorbent resin powder (e) thus obtained was mixed with 3.55 parts by weight of a surface cross-linking agent composed of 0.51 parts by weight of propylene glycol, 0.31 parts by weight of 1,4-butane diol, and 2.73 parts by weight of water. A water-absorbent resin (5) was obtained by subjecting the resultant mixture to a heat treatment at 200°C for 40 minutes. The results are shown in Table 1.

[0135]

[Referential Example 6]

15 A reaction solution was formed by dissolving 5.6 g of polyethylene glycol diacrylate (average addition mol number of ethylene oxide 8) in 6600 g of sodium acrylate aqueous solution (monomer concentration 38 mass%) having a neutralizing ratio of 72 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 3.42 g of sodium persulfate and 0.017 g of L-ascorbic acid were added to the stirred reaction solution, polymerization was started about one minute thereafter. The polymerization was carried out at 30°C - 90°C. A polymer of the hydrogel form was extracted from the reaction vessel 40 minutes thereafter. The hydrogel polymer thus obtained was finely divided into particles about 1 - 4 mm in diameters. This hydrogel polymer was spread on a 50-mesh metal sheet (having a mesh size of 300 μ m). Then, the hydrogel polymer was dried and pulverized in

the same manner as in the Referential Example 1, and classified with a metal sheet having an aperture of 20 mesh (having a mesh size of 850 μm). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (f).

100 parts by weight of the water-absorbent resin powder (f) thus obtained was mixed with 3.55 parts by weight of a surface cross-linking agent having the same composition as in Referential Example 5. A water-absorbent resin (6) was obtained by 10
subjecting the resultant mixture to a heat treatment at 200°C for 50 minutes. The results are shown in Table 1.

[0136]

[Referential Example 7]

A reaction solution was formed by dissolving 3.1 g of 15
polyethylene glycol diacrylate (average addition mol number of ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 33 mass%) having a neutralizing ratio of 65 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same 20
reaction vessel as in Referential Example 1. The system having the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 2.46 g of sodium persulfate and 0.10 g of L-ascorbic acid were added to the stirred reaction solution, polymerization 25
was started about one minute thereafter. The polymerization was carried out at 30°C - 85°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes thereafter. The hydrogel polymer thus obtained was finely divided into particles about 1 - 4 mm in diameters. This hydrogel polymer 30
was spread on a 50-mesh metal sheet (having a mesh size of 300 μm). Then, the hydrogel polymer was dried and pulverized in the same manner as in the Referential Example 1, and classified

with a metal sheet having an aperture of 20 mesh (having a mesh size of 850 μm). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (g).

5 100 parts by weight of the water-absorbent resin powder (g) thus obtained was mixed with 3.83 parts by weight of a surface cross-linking agent having the same composition as in Referential Example 1. A water-absorbent resin (7) was obtained by
10 subjecting the resultant mixture to a heat treatment at 195°C for 60 minutes. The results are shown in Table 1.

[0137]

[Referential Example 8]

A reaction solution was formed by dissolving 6.8 g of polyethylene glycol diacrylate (average addition mol number of
15 ethylene oxide 8) in 5500 g of sodium acrylate aqueous solution (monomer concentration 20 mass%) having a neutralizing ratio of 30 mol%. Then, this reaction solution was deaerated in the same manner as in Referential Example 1 and supplied to the same reaction vessel as in Referential Example 1. The system having
20 the reaction solution kept at 30°C was displaced with nitrogen gas. Subsequently, when the reaction solution was continuously stirred and 2.46 g of sodium persulfate and 0.10 g of L-ascorbic acid were added to the stirred reaction solution, polymerization was started about one minute thereafter. The polymerization
25 was carried out at 30°C - 80°C. A polymer of the hydrogel form was extracted from the reaction vessel 60 minutes thereafter. The hydrogel polymer thus obtained was finely divided into particles about 1 - 4 mm in diameters. This finely divided hydrogel polymer was spread on a 50-mesh metal sheet (having
30 a mesh size of 300 μm). Then, the hydrogel polymer was dried and pulverized in the same manner as in the Referential Example 1, and classified with a metal sheet having an aperture of 20

mesh (having a mesh size of 850 μm). And, the classified particles were blended to obtain an amorphously pulverized water-absorbent resin powder (h).

100 parts by weight of the water-absorbent resin powder (h) thus obtained was mixed with 3.8 parts by weight of a surface cross-linking agent having the same composition as in Referential Example 2. A water-absorbent resin (8) was obtained by subjecting the resultant mixture to a heat treatment at 210°C for 50 minutes. The results are shown in Table 1.

10 [0138]

[Referential Example 9]

An amorphously pulverized water-absorbent resin powder (i) was obtained by following the procedure of Referential Example 1. The water-absorbent resin powder (i) thus obtained was labeled in its unmodified form as "absorbent resin (9)." The results are shown in Table 1.

[0139]

[Referential Example 10]

In a beaker having an inner volume of 5 L, 1 L of purified water was placed and then stirred and retained by heating at a temperature of 60°C. Then, 2 L of an aqueous solution having 114.5 parts by weight of zinc sulfate (made by Wako Pure Chemical Industries, Ltd.) and 17.6 parts by weight of sodium silicate powder (made by Wako Pure Chemical Industries, Ltd.) mixed therein and an ammonia aqueous solution were added dropwise to the purified water heedfully so as to retain the pH value at 7.5. A complex oxide hydrate containing zinc and silicate (B1) (mass ratio of zinc and silicon: 85/15) was obtained by separating the resultant precipitate by filtration, washing the separated precipitate, and drying the washed precipitate at 120°C for six hours.

30 [0140]

[Referential Example 11]

In a beaker having an inner volume of 5 L, 1 L of purified water was placed and then stirred and retained by heating at a temperature of 60°C. Then, 2 L of an aqueous solution having 132.9 parts by weight of zinc sulfate (made by Wako Pure Chemical Industries, Ltd.) and 110.1 parts by weight of aluminum sulfate 14 - 18 hydrate (made by Wako Pure Chemical Industries, Ltd.) mixed therein and an aqueous ammonia solution were added dropwise to the purified water heedfully so as to retain the pH value at 7.5. A complex oxide hydrate containing zinc and aluminum (B2) (mass ratio of zinc and aluminum 85/15) was obtained by separating the resultant precipitate by filtration, washing the separated precipitate, and drying the washed precipitate at 120°C for six hours.

[0141]

15 [Referential Example 12]

In a beaker having an inner volume of 5 L, 1 L of purified water was placed and then stirred and retained by heating at a temperature of 60°C. Then, 2 L of an aqueous solution having 161.2 parts by weight of titanium chloride (made by Wako Pure Chemical Industries, Ltd.) and 9.1 parts by weight of sodium silicate powder (made by Wako Pure Chemical Industries, Ltd.) mixed therein and an ammonia aqueous solution were added dropwise to the purified water heedfully so as to retain the pH value at 7.5. A complex oxide hydrate containing titanium and silicon (B3) (mass ratio of titanium and silicon: 91/9) was obtained by separating the resultant precipitate by filtration, washing the separated precipitate, and drying the washed precipitate at 120°C for six hours.

[0142]

30 [Example 1]

A water-absorbent resin composition (1) was obtained by adding 100 parts by weight of the water-absorbent resin (1)

obtained in Referential Example 1 and 0.50 mass part of a complex
oxide hydrate of zinc and silicon (mass ratio of contents of
zinc and silicon: 82/18 and average particle diameter: 0.36 μm ;
made by Titan Kogyo K.K. and sold under the trademark designation
5 of "Ceratiox SZ-100S") together and mixing them (dry blend).

[0143]

The water-absorbent resin composition (1) consequently
obtained was tested for absorption capacity without load,
absorption capacity under the pressure of 1.9 kPa, ability to
10 deodorize hydrogen sulfide, ability to deodorize ammonia,
performance of deodorization, separation ratio, and hygroscopic
blocking ratio. The results are shown in Table 2, Table 3, and
Table 4.

[0144]

15 [Example 2]

A water-absorbent resin composition (2) was obtained by
following the procedure of Example 1 while changing the
water-absorbent resin (1) obtained in Referential Example 1 to
the water-absorbent resin (2) obtained in Referential Example
20 2. The water-absorbent resin composition (2) was tested in the
same manner as in Example 1. The results are shown in Table
2 and Table 3.

[0145]

[Example 3]

25 A water-absorbent resin composition (3) was obtained by
following the procedure of Example 1 while changing the
water-absorbent resin (1) obtained in Referential Example 1 to
the water-absorbent resin (3) obtained in Referential Example
3. The water-absorbent resin composition (3) was tested in the
30 same manner as in Example 1. The results are shown in Table
2 and Table 3.

[0146]

[Example 4]

A water-absorbent resin composition (4) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (4) obtained in Referential Example 4. The water-absorbent resin composition (4) was tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0147]

10 [Example 5]

A water-absorbent resin composition (5) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (5) obtained in Referential Example 5. The water-absorbent resin composition (5) was tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0148]

[Example 6]

20 A water-absorbent resin composition (6) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (6) obtained in Referential Example 6. The water-absorbent resin composition (6) was tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0149]

[Example 7]

30 A water-absorbent resin composition (7) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (5) obtained in Referential Example

5 and additionally using 0.5 parts by weight of 15 mass% aqueous solution of the extract from leaves of a theaceous plants (sold by Shiraimatsu Shinyaku K.K. [located at 37-1 Ugawa, Mizuguchi-town, Koga-country, Shiga-prefecture] under the product code of "FS-80MO") as a plant component. The water-absorbent resin composition (7) was tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0150]

10 [Example 8]

A water-absorbent resin composition (8) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to the complex oxide hydrate of zinc and silicon (B1) (mass ratio of zinc and silicon: 90/10) obtained in Referential Example 10. The water-absorbent resin composition (8) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0151]

[Example 9]

20 A water-absorbent resin composition (9) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to the complex oxide hydrate of zinc and aluminum (B2) (mass ratio of zinc and aluminum: 90/10) obtained in Referential Example 1. The water-absorbent resin composition (9) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0152]

[Example 10]

30 A water-absorbent resin composition (10) was obtained by following the procedure of Example 1 while changing the amount of the complex oxide hydrate of zinc and silicon to 0.10 parts byweight. The water-absorbent resin composition (10) was tested

in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0153]

[Comparative Example 1]

5 A comparative water-absorbent resin composition (1) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (7) obtained in Referential Example 7. The comparative water-absorbent resin composition (1) was
10 tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0154]

[Comparative Example 2]

15 A comparative water-absorbent resin composition (2) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (8) obtained in Referential Example 8. The comparative water-absorbent resin composition (2) was
20 tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0155]

[Comparative Example 3]

25 A comparative water-absorbent resin composition (3) was obtained by following the procedure of Example 1 while changing the water-absorbent resin (1) obtained in Referential Example 1 to the water-absorbent resin (9) obtained in Referential Example 9. The comparative water-absorbent resin composition (3) was
30 tested in the same manner as in Example 1. The results are shown in Table 2 and Table 3.

[0156]

[Comparative Example 4]

A comparative water-absorbent resin composition (4) was

obtained by following the procedure of Example 1 while omitting the addition of the complex oxide hydrate of zinc and silicon. The comparative water-absorbent resin composition (4) was tested in the same manner as in Example 1. The results are shown in
5 Table 2, Table 3, and Table 4.

[0157]

[Comparative Example 5]

A comparative water-absorbent resin composition (5) was obtained by following the procedure of Example 1 while changing
10 the complex oxide hydrate of zinc and silicon to a complex oxide hydrate having a different mass ratio of contents of zinc and silicon and a different particle diameter (mass ratio of contents of zinc and silicon: 40/60, particle diameter: not more than 250 μm : made by Rasa Kogyo K.K. and sold under the trademark
15 designation of "Shukurenzu KD-211S"). The comparative water-absorbent resin composition (5) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0158]

20 [Comparative Example 6]

A comparative water-absorbent resin composition (6) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to a complex oxide hydrate having a different mass ratio of contents of zinc and
25 silicon and a different particle diameter (mass ratio of contents of zinc and silicon: 40/60, particle diameter: not more than 1 μm : made by Rasa Kogyo K.K. and sold under the trademark designation of "Shukurenzu KD-211G"). The comparative water-absorbent resin composition (6) was tested in the same
30 manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0159]

[Comparative Example 7]

A comparative water-absorbent resin composition (7) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to a complex oxide hydrate having a different combination of metal elements, i.e. titanium and zinc (mass ratio of contents of titanium and zinc: 50/50, average particle diameter: 0.50 μ m: made by Titan Kogyo K.K. and sold under the trademark designation of "Ceratiox TZ-100"). The comparative water-absorbent resin composition (7) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0160]

[Comparative Example 8]

A comparative water-absorbent resin composition (8) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to a basic zinc carbonate as a zinc compound (made by Wako Pure Chemical Industries, Ltd.). The comparative water-absorbent resin composition (8) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0161]

[Comparative Example 9]

A comparative water-absorbent resin composition (9) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to zinc oxide, which is oxide of only zinc, (average particle diameter: 31 nm: made by CI Kasei K.K. and sold under the trademark designation of "Nanotec ZnO"). The comparative water-absorbent resin composition (9) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0162]

[Comparative Example 10]

A comparative water-absorbent resin composition (10) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to silicon dioxide, which is oxide of only silicon, (average particle diameter: 26 nm: made by CI Kasei K.K. and sold under the trademark designation of "Nanotec SiO₂"). The comparative water-absorbent resin composition (10) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0163]

10 [Comparative Example 11]

A comparative water-absorbent resin composition (11) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to titanium dioxide, which is oxide of only titanium, (average particle diameter: 30 nm: made by CI Kasei K.K. and sold under the trademark designation of "Nanotec TiO₂"). The comparative water-absorbent resin composition (11) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

20 [0164]

[Comparative Example 12]

A comparative water-absorbent resin composition (12) was obtained by following the procedure of Example 1 while changing the complex oxide hydrate of zinc and silicon to the complex oxide hydrate (B3) of titanium and silicon obtained in Referential Example 12. The comparative water-absorbent resin composition (12) was tested in the same manner as in Example 1. The results are shown in Table 2, Table 3, and Table 4.

[0165]

30 [Comparative Example 13]

A comparative water-absorbent resin composition (12) was obtained by following the procedure of Example 1 while changing

the complex oxide hydrate of zinc and silicon to the mixture of the zinc oxide and the silicon dioxide (obtained by mixing the zinc oxide and the silicon dioxide at a ratio of 1/1). The comparative water-absorbent resin composition (12) was tested for absorption capacity without load, absorption capacity under the pressure of 1.9 kPa, performance of deodorization of hydrogen sulfide, property of deodorizing ammonia, and deodorization. The results are shown in Table 2 and Table 3.

[0166]

10 [Example 11]

In a mixer, 37 parts by weight of the water-absorbent resin composition (1) obtained in Example 1 and 63 parts by weight of ground wood pulp were dry mixed. Then, the resultant mixture was pneumatically spread on a wire screen formed in an aperture of 400 mesh (mesh size 38 μm) by the use of a batch type pneumatic sheet producing device. Consequently, a web measuring 130 mm \times 400 mm was obtained. When this web was pressed under the pressure of 196.14 kPa for five seconds, it produced an absorbent material having a basis weight of about 0.05 g/cm².

20 [0167]

Then, a pad type adult disposable diaper as an absorbent product was obtained by pasting a liquid-impermeable backsheet made of liquid-impermeable polypropylene, the absorbent material mentioned above, and a topsheet of non-woven fabric made of a liquid-permeable polypropylene sequentially in the order mentioned. This absorbent product (1) had a mass of 50 g.

[0168]

The absorbent product (1) was tested for deodorizing property. The results are shown collectively in Table 5.

30 [0169]

[Examples 12 - 14]

Absorbent products (2), (3), and (4) were obtained by

following the procedure of Example 11 while changing the water-absorbent resin composition (1), respectively to the water-absorbent resin compositions (8), (9), and (10).

[0170]

- 5 The absorbent products (2), (3), and (4) thus obtained were tested for deodorizing property. The results are shown collectively in Table 5.

[0171]

[Comparative Examples 14 - 17]

- 10 The comparative absorbent products (1), (2), (3), and (4) were obtained by following the procedure of Example 10 while changing the water-absorbent resin composition (1) respectively to the comparative water-absorbent resin compositions (4), (5), (7), and (13) obtained in Comparative Examples 4, 5, 7, and 13.

- 15 [0172]

The comparative absorbent products (1), (2), (3), and (4) thus obtained were tested for deodorizing property. The results are shown collectively in Table 5.

[0173]
[Table 1]

	Water-absorbent resin	Absorption	Absorption capacity under the pressure of 1.9 KPa (g/g)	Particle diameter distribution (mass%)				
		capacity without load (g/g)	(g/g)	850 μ m \leq	600 μ m \leq <850 μ m	300 μ m \leq <600 μ m	150 μ m \leq <300 μ m	<150 μ m
Referential Example 1	Water-absorbent resin (1)	35	32	0	16	58	22	4
Referential Example 2	Water-absorbent resin (2)	31	30	0	14	70	15	2
Referential Example 3	Water-absorbent resin (3)	35	32	0	17	65	16	2
Referential Example 4	Water-absorbent resin (4)	34	31	0	20	65	14	1
Referential Example 5	Water-absorbent resin (5)	33	30	0	23	60	15	2
Referential Example 6	Water-absorbent resin (6)	26	27	0	23	58	17	2
Referential Example 7	Water-absorbent resin (7)	42	12	0	3	52	37	8
Referential Example 8	Water-absorbent resin (8)	22	18	0	13	69	16	2
Referential Example 9	Water-absorbent resin (9)	45	13	0	16	58	22	4

[0174]
[Table 2]

	Water-absorbent resin composition	Absorption capacity without load (g/g)	Absorption capacity under the pressure of 1.9 KPa (g/g)	Amount of the hydrogen sulfide residue under wet (ppm)			Amount of wet ammonia residue (ppm)		
				30min	60min	180min	10min	30min	60min
Example 1	Water-absorbent resin composition (1)	36	32	2.0	1.0	0.0	220	90	60
Example 2	Water-absorbent resin composition (2)	31	30	2.5	1.5	1.0	120	40	10
Example 3	Water-absorbent resin composition (3)	35	32	2.5	1.5	1.0	100	20	5
Example 4	Water-absorbent resin composition (4)	34	31	3.0	2.0	1.5	90	30	5
Example 5	Water-absorbent resin composition (5)	33	30	3.0	1.5	0.0	120	40	15
Example 6	Water-absorbent resin composition (6)	26	27	2.5	1.0	0.0	180	70	50
Example 7	Water-absorbent resin composition (7)	33	30	2.0	1.5	0.0	120	40	15
Example 8	Water-absorbent resin composition (8)	34	28	2.0	1.0	0.0	200	80	60
Example 9	Water-absorbent resin composition (9)	34	28	2.5	1.5	0.5	210	80	60
Example 10	Water-absorbent resin composition (10)	36	31	6.0	5.0	5.0	250	80	70
Comparative Example 1	Comparative water-absorbent resin composition (1)	42	12	11.0	8.0	6.0	230	150	100

[Table 2 (continued)]

Comparative Example 2	Comparative water-absorbent resin composition(2)	22	18	10.0	8.0	7.0	200	130	60
Comparative Example 3	Comparative water-absorbent resin composition(3)	45	13	11.0	9.0	7.0	250	120	60
Comparative Example 4	Comparative water-absorbent resin composition(4)	35	31	15.0	14.5	14.0	430	110	50
Comparative Example 5	Comparative water-absorbent resin composition(5)	35	30	10.5	7.0	3.0	300	110	70
Comparative Example 6	Comparative water-absorbent resin composition(6)	35	29	8.0	4.5	1.5	280	120	75
Comparative Example 7	Comparative water-absorbent resin composition(7)	34	28	7.5	6.5	5.0	300	130	100
Comparative Example 8	Comparative water-absorbent resin composition(8)	34	27	12.0	10.5	9.5	400	150	80
Comparative Example 9	Comparative water-absorbent resin composition(9)	35	30	11.0	9.5	8.0	410	140	90
Comparative Example 10	Comparative water-absorbent resin composition(10)	35	25	14.5	14.5	13.5	230	90	60
Comparative Example 11	Comparative water-absorbent resin composition(11)	33	29	14.5	14.5	13.0	350	130	80
Comparative Example 12	Comparative water-absorbent resin composition(12)	33	28	15.5	15.5	14.0	360	120	80
Comparative Example 13	Comparative water-absorbent resin composition(13)	34	26	11.5	10.0	9.0	240	110	70

[0175]

[Table 3]

	Water-absorbent resin composition	Deodorizing test			
		0 hour later	3 hours later	6 hours later	24 hours later
Example 1	Water-absorbent resin composition (1)	1.2	2.2	2.6	3.0
Example 2	Water-absorbent resin composition (2)	1.3	2.2	2.5	3.0
Example 3	Water-absorbent resin composition (3)	1.1	2.4	2.6	3.1
Example 4	Water-absorbent resin composition (4)	1.3	2.3	2.5	3.1
Example 5	Water-absorbent resin composition (5)	1.4	2.2	2.4	3.0
Example 6	Water-absorbent resin composition (6)	1.3	2.4	2.7	3.0
Example 7	Water-absorbent resin composition (7)	1.2	2.0	2.5	2.8
Example 8	Water-absorbent resin composition (8)	1.3	2.2	2.5	2.9
Example 9	Water-absorbent resin composition (9)	1.3	2.4	2.6	3.0
Example 10	Water-absorbent resin composition (10)	1.8	2.6	2.9	3.2
Comparative Example 1	Comparative water-absorbent resin composition(1)	3.3	3.7	3.9	4.1
Comparative Example 2	Comparative water-absorbent resin composition(2)	4.2	4.4	4.5	4.8

[Table 3 (continued)]

Comparative Example 3	Comparative water-absorbent resin composition(3)	4.0	4.2	4.5	4.7
Comparative Example 4	Comparative water-absorbent resin composition(4)	4.7	4.7	4.8	4.5
Comparative Example 5	Comparative water-absorbent resin composition(5)	2.3	3.7	3.7	3.5
Comparative Example 6	Comparative water-absorbent resin composition(6)	3.0	4.0	4.2	3.5
Comparative Example 7	Comparative water-absorbent resin composition(7)	2.3	3.3	3.8	4.0
Comparative Example 8	Comparative water-absorbent resin composition(8)	2.7	3.4	3.8	4.0
Comparative Example 9	Comparative water-absorbent resin composition(9)	2.7	3.3	3.9	4.2
Comparative Example 10	Comparative water-absorbent resin composition(10)	3.8	3.7	4.3	4.4
Comparative Example 11	Comparative water-absorbent resin composition(11)	3.3	3.4	3.4	4.4
Comparative Example 12	Comparative water-absorbent resin composition(12)	2.7	2.9	3.7	3.9
Comparative Example 13	Comparative water-absorbent resin composition(13)	2.0	3.2	3.2	3.0

[0176]

[Table 4]

	Water-absorbent resin composition	Separation ratio (%)	Hygroscopic blocking ratio(mass%)
Example 1	Water-absorbent resin composition (1)	0	0
Example 8	Water-absorbent resin composition (8)	0	0
Example 9	Water-absorbent resin composition (9)	0	0
Example 10	Water-absorbent resin composition (10)	0	0
Comparative Example 4	Comparative water-absorbent resin composition(4)	-	100
Comparative Example 5	Comparative water-absorbent resin composition(5)	0	100
Comparative Example 6	Comparative water-absorbent resin composition(6)	21	100
Comparative Example 7	Comparative water-absorbent resin composition(7)	100	39.7
Comparative Example 8	Comparative water-absorbent resin composition(8)	38	0
Comparative Example 9	Comparative water-absorbent resin composition(9)	0	0
Comparative Example 10	Comparative water-absorbent resin composition(10)	100	0
Comparative Example 11	Comparative water-absorbent resin composition(11)	100	98.8
Comparative Example 12	Comparative water-absorbent resin composition(12)	100	51.3

[0177]

[Table 5]

	Water-absorbent product	Deodorizing test			
		0 hour later	3 hours later	6 hours later	24 hours later
Example 11	Water-absorbent product (1)	1.2	2.0	2.4	2.8
Example 12	Water-absorbent product (2)	1.2	1.9	2.2	2.5
Example 13	Water-absorbent product (3)	1.2	1.9	2.2	2.5
Example 14	Water-absorbent product (4)	1.2	2.2	2.6	3.0
Comparative Example 14	Comparative water-absorbent product (1)	4.5	4.5	4.7	4.8
Comparative Example 15	Comparative water-absorbent product (2)	2.5	3.6	3.7	4.0
Comparative Example 16	Comparative water-absorbent product (3)	2.0	3.2	3.7	4.1
Comparative Example 17	Comparative water-absorbent product (4)	2.3	35.0	3.6	3.6

[Name of Document] Abstract

[Abstract]

[Problem] An object of this invention is to provide a water-absorbent resin composition, an absorbent material, and
5 an absorbent product, and a method for production of a water-absorbent resin composition, which relate to a water-absorbent resin composition including a water-absorbent resin and an additive, which have a low ratio of separation of additives (low separation ratio), excel in the hygroscopic and
10 fluid property (fluid property of a powder after water-absorbent resin or water-absorbent resin absorbed water) and in the deodorizing property (especially, odor originating in sulfur compounds such as hydrogen disulfide or mercaptan), and also excel in the absorbent property.

15 [Solving Means] The water-absorbent resin composition of the present invention comprises (A) cross-linked absorbent resin obtainable by polymerizing an unsaturated monomer having an acid group and/or a salt thereof as main component; and (B) complex oxide hydrate containing (b1) zinc and silicon, or (b2)
20 zinc and aluminum, wherein the complex oxide hydrate contains zinc as main metal component, the mass ratio of the content of zinc and the content of silicon or aluminum is in the range of 50/50 - 99/1, and the absorption capacity at 60 minutes toward 0.90 mass% sodium chloride aqueous solution under the pressure
25 of 1.9 kPa is not less than 20 g/g.

[Selected Figure] none

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